

UNIVERSITY OF SWAZILAND

FACULTY OF SCIENCE AND ENGINEERING

DEPARTMENT OF PHYSICS

MAIN EXAMINATION 2012/2013

TITLE OF PAPER : ELECTROMAGNETIC THEORY

COURSE NUMBER : P331

TIME ALLOWED : THREE HOURS

**INSTRUCTIONS : ANSWER ANY FOUR OUT OF FIVE
QUESTIONS.
EACH QUESTION CARRIES 25 MARKS.**

**MARKS FOR DIFFERENT SECTIONS ARE
SHOWN IN THE RIGHT-HAND MARGIN.**

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GIVEN BY THE INVIGILATOR.**

P331 ELECTROMAGNETIC THEORY

Question one

- (a) (i) For any closed surface S , enclosing a volume V , the integral form of continuity equation for electric charges in Electromagnetic theory can be written as

$$\oint_S \vec{J} \cdot d\vec{s} = -\frac{d}{dt} \left(\int_V \rho_v dV \right) .$$

Explain briefly the meaning of the left hand side

and the right hand side of this equation and indicate which law in physics it describes. **(3+1 marks)**

- (ii) Use the divergence theorem to transform the above integral form of continuity equation for electric charges into its differential form. **(3 marks)**

- (iii) (A) Show that without introducing the displacement current term, i.e., $\frac{\partial \vec{D}}{\partial t}$,

in the equation for Ampere's law, i.e., $\vec{\nabla} \times \vec{H} = \vec{J}$ instead of

$$\vec{\nabla} \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} ,$$

Maxwell's equations would contradict the

continuity equation for electric charges. **(2 marks)**

- (B) Show that by including the displacement current term, Maxwell's equations are in agreement with the continuity equation. **(4 marks)**

- (b) (i) From the time-independent Maxwell's equations deduce the following Poisson's equation for the electric scalar potential f in free space as

$$\nabla^2 f = -\frac{\rho_v}{\epsilon_0} \quad \text{where} \quad \vec{E} \equiv -\vec{\nabla} f \quad \textbf{(3 marks)}$$

- (ii) The Pointing vector $\vec{R} \equiv \vec{r} - \vec{r}' \equiv \vec{e}_R R$ is from the source point

$\vec{r}' \equiv \vec{e}_x x' + \vec{e}_y y' + \vec{e}_z z'$ toward the field point $\vec{r} \equiv \vec{e}_x x + \vec{e}_y y + \vec{e}_z z$. By direct

evaluation of $\vec{\nabla} \left(\frac{1}{R} \right)$ where

$$\begin{cases} R = \sqrt{(x-x')^2 + (y-y')^2 + (z-z')^2} \\ \vec{\nabla} \rightarrow \vec{e}_x \frac{\partial}{\partial x} + \vec{e}_y \frac{\partial}{\partial y} + \vec{e}_z \frac{\partial}{\partial z} \\ \vec{e}_R = \vec{e}_x \frac{(x-x')}{R} + \vec{e}_y \frac{(y-y')}{R} + \vec{e}_z \frac{(z-z')}{R} \end{cases}$$

show that $\vec{\nabla} \left(\frac{1}{R} \right) = -\vec{e}_R \frac{1}{R^2}$. **(6 marks)**

- (iii) Assuming the solution for the Poisson's equation in (b)(i) is

$$f(x, y, z) = \iiint_{\text{source points}} \frac{\rho_v(x', y', z')}{4\pi\epsilon_0 R} dx' dy' dz' ,$$

use the result in (b)(ii) and

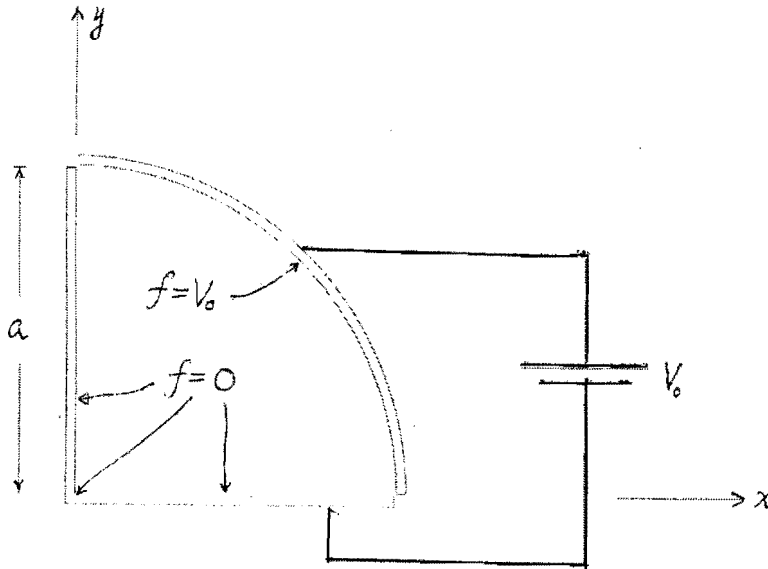
$\vec{E} \equiv -\vec{\nabla} f$ to deduce that

$$\vec{E}(x, y, z) = \iiint_{\text{source points}} \left(\vec{e}_R \frac{\rho_v(x', y', z')}{4\pi\epsilon_0 R^2} \right) dx' dy' dz' \quad \text{which is just the}$$

Coulomb's law. **(3 marks)**

Question two

A V – tube capacitor is extended very long into z direction with its cross section as shown below:



The electric potential $f(\rho, \phi)$ in cylindrical coordinates for the region between two conductors, i.e., $0 \leq \rho \leq a$ & $0 \leq \phi \leq \frac{\pi}{2}$, satisfies the following two dimensional Laplace equation :

$$\rho \frac{\partial}{\partial \rho} \left(\rho \frac{\partial f(\rho, \phi)}{\partial \rho} \right) + \frac{\partial^2 f(\rho, \phi)}{\partial \phi^2} = 0$$

- (a) (i) Set $f(\rho, \phi) = F(\rho) G(\phi)$ and use separation variable scheme to deduce the following two ordinary differential equations :

$$\begin{cases} \rho \frac{d}{d\rho} \left(\rho \frac{dF(\rho)}{d\rho} \right) = -k F(\rho) & \dots\dots (1) \\ \frac{d^2 G(\phi)}{d\phi^2} = k G(\phi) & \dots\dots (2) \end{cases}$$

where k is a separation constant of any value. (4 marks)

- (ii) Based on eq.(2), i.e., differential equation for ϕ , explain why the eigenvalues for k are $k = -m^2$ where $m = 1, 2, 3, \dots$ (3 marks)

- (iii) By direct substitution, show that ρ^m & ρ^{-m} are the two independent solution to eq.(1) with $k = -m^2$. (3 marks)

Question two (continued)

(b) The general solution for (a) is

$$f(\rho, \phi) = \sum_{m=1}^{\infty} f_m(\rho, \phi)$$

$$= \sum_{m=1}^{\infty} (A_m \rho^m + B_m \rho^{-m}) (C_m \cos(m\phi) + D_m \sin(m\phi)) \dots\dots (3)$$

where A_m , B_m , C_m & D_m are arbitrary constants. This general solution is subjected to the following four boundary conditions :

$$BC(1) : f_m(0, \phi) = 0 \quad \forall \quad 0 \leq \phi \leq \frac{\pi}{2}$$

$$BC(2) : f_m(\rho, 0) = 0 \quad \forall \quad 0 \leq \rho \leq a$$

$$BC(3) : f_m(\rho, \frac{\pi}{2}) = 0 \quad \forall \quad 0 \leq \rho \leq a$$

$$BC(4) : f(a, \phi) = V_0 \quad \forall \quad 0 \leq \phi \leq \frac{\pi}{2}$$

(i) Apply BC(1) and deduce from eq.(3) that

$$f(\rho, \phi) = \sum_{m=1}^{\infty} (A_m \rho^m) (C_m \cos(m\phi) + D_m \sin(m\phi)) \dots\dots (4) \quad (2 \text{ marks})$$

(ii) Apply BC(2) and deduce from eq.(4) that

$$f(\rho, \phi) = \sum_{m=1}^{\infty} (A_m \rho^m) (D_m \sin(m\phi)) \text{ name } (A_m D_m) \text{ as } E_m$$

$$= \sum_{m=1}^{\infty} (E_m \rho^m \sin(m\phi)) \dots\dots (5) \quad (2 \text{ marks})$$

(iii) Apply BC(3) and deduce from eq.(5) that

$$f(\rho, \phi) = \sum_{n=1}^{\infty} (F_n \rho^{2n} \sin(2n\phi)) \dots\dots (6) \quad (3 \text{ marks})$$

where $F_n \equiv E_{2n}$ & $n = 1, 2, 3, \dots\dots$

(iv) Apply BC(4) and find the values of F_n in terms of V_0 , a & n and show that

$$F_n = \frac{2 V_0 (1 - \cos(n\pi))}{n \pi a^{2n}} \quad n = 1, 2, 3, \dots\dots \quad (8 \text{ marks})$$

(Hint : $\int_{\phi=0}^{\frac{\pi}{2}} \sin(2n\phi) \sin(2m\phi) d\phi = \begin{cases} 0 & \text{if } n \neq m \\ \frac{\pi}{4} & \text{if } n = m \end{cases}$)

Question three

(a) The point form of Ohm's law in a conductive region of conductivity σ is $\vec{J} = \sigma \vec{E}$ where \vec{J} & \vec{E} are the current density and electric field respectively. Show that it can lead to the commonly known Ohm's law $V = IR$ for a conducting wire of length L , cross-sectional area A , total flowing current I and the terminal voltage across the wire V where $R = \frac{L}{\sigma A}$. (5 marks)

(b) According to modified Drude's model of electric conduction in the conductive material with conductivity σ under the applied electric field \vec{E} , the equation of motion for an average conduction electron in the conductor is

$$m_e \frac{d\vec{v}_d}{dt} = -e \vec{E} - \frac{2 m_e \vec{v}_d}{\tau_c} \dots\dots (1) \text{ where } (-e) \text{ \& } m_e \text{ are the charge and mass of an electron respectively.}$$

(i) Explain briefly the meaning of \vec{v}_d , τ_c & $\left(-\frac{2 m_e \vec{v}_d}{\tau_c}\right)$ in the above equation. (4 marks)

(ii) In the steady state situation, i.e., $\frac{d\vec{v}_d}{dt} = 0$, use the equation of motion and the point form of Ohm's law to deduce that

$$\sigma = \frac{n e^2}{2 m_e} \tau_c \text{ where } n \equiv \text{number density of conduction electrons} .$$

(Hint : $\vec{J} = \rho_v \vec{v}_d = -n e \vec{v}_d$) (6 marks)

(iii) The pure metal potassium K possesses the following data at room temperature as atomic number = 39.098, density = 871 $\frac{kg}{m^3}$ and

$$\text{conductivity} = 1.4 \times 10^7 \frac{1}{\Omega m}$$

(A) Calculate the number density of conduction electrons of the metal potassium with the knowledge of each potassium atom contributes one conduction electron. (3 marks)

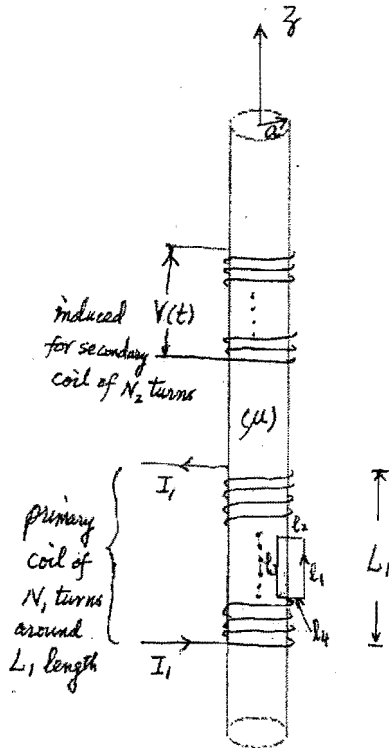
(B) Find the value of τ_c for metal potassium at room temperature.

(Hint : Avogadro number = $6.023 \times 10^{26} \frac{\text{atoms}}{\text{kg - mole}}$) (3 marks)

(iv) In the time-harmonic situation, i.e., $\vec{E} = \vec{e}_E E_0 \cos(\omega t) = \vec{e}_E \text{Re}\{E_0 e^{i\omega t}\}$, set $\vec{v}_d = \vec{e}_E v_d \cos(\omega t + \phi) = \vec{e}_E \text{Re}\{\hat{v}_d e^{i\omega t}\}$ where $\hat{v}_d \equiv v_d e^{i\phi}$, use eq. (1) to deduce that $\hat{v}_d = -\frac{e \tau_c}{2 m_e + i \omega m_e \tau_c} E_0$. (4 marks)

Question four

- (a) A static current I_1 flows in the N_1 turn toroid wired around an iron core of cross section radius a and permeability μ , with its central axis coinciding with the z -axis as shown below:



- (i) Use the closed loop $(l_1 + l_2 + l_3 + l_4)$ drawn in the given diagram where $\vec{l}_1 = \vec{e}_z b$ (outside the core), $\vec{l}_2 = -\vec{e}_\rho c$, $\vec{l}_3 = -\vec{e}_z b$ (inside the core) & $\vec{l}_4 = \vec{e}_\rho c$, set $\vec{B} = \vec{e}_z B_z(\rho)$ for $\rho \leq a$ & $\vec{B} = 0$ for $\rho > a$ and use the integral form of Ampere's law to find \vec{B} and show that $\vec{B} = \vec{e}_z \frac{\mu N_1}{L_1} I_1$ for $\rho \leq a$. (5 marks)
- (ii) Assuming the same \vec{B} obtained in (a)(i) is maintained throughout the iron core (which is a good assumption when $\mu \gg \mu_0$), find the total magnetic flux Ψ_m passing through the cross-section area πa^2 of the iron core, i.e., $\Psi_m = \int \vec{B} \cdot d\vec{s}$ where $d\vec{s} = \vec{e}_z \rho d\rho d\phi$, $0 \leq \rho \leq a$ & $0 \leq \phi \leq 2\pi$, and show that $\Psi_m = \frac{\mu N_1 \pi a^2}{L_1} I_1$. (2 marks)

Question four (continued)

- (iii) Find the mutual inductance M between the primary and secondary coils and the self-inductance L_1 of the primary coil in terms of a, L_1, N_1, N_2 & μ .

(3 marks)

(Hint : The total magnetic flux passing through the primary and secondary coils are $N_1 \Psi_m$ & $N_2 \Psi_m$ respectively where Ψ_m is obtained in (a)(ii))

- (iv) Find the induced e.m.f. $V(t)$ of the secondary coil in terms of $a, L_1, N_1, N_2, \mu, I_0$ & ω if the primary coil carries a sinusoidal current of $I_0 \sin(\omega t)$ instead of carrying a static current I_1 .

(2 marks)

- (b) The Maxwell's equations for the material region of parameters μ, ϵ & σ are

$$\vec{\nabla} \cdot \vec{E} = 0 \quad \dots\dots (1)$$

$$\vec{\nabla} \cdot \vec{B} = 0 \quad \dots\dots (2)$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \quad \dots\dots (3)$$

$$\vec{\nabla} \times \vec{B} = \mu \sigma \vec{E} + \mu \epsilon \frac{\partial \vec{E}}{\partial t} \quad \dots\dots (4)$$

- (i) Deduce from them the following wave equation for \vec{E} as

$$\nabla^2 \vec{E} - \mu \sigma \frac{\partial \vec{E}}{\partial t} - \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2} = 0 \quad \dots\dots (5) \quad . \quad \text{(4 marks)}$$

- (ii) Set \vec{E} as $\left(\vec{E}(\text{space}) e^{i\omega t} \right)$ and substitute it into the above wave equation,

to deduce the following time-harmonic equation for $\vec{E}(\text{space})$ as

$$\nabla^2 \vec{E}(\text{space}) - \hat{\gamma}^2 \vec{E}(\text{space}) = 0 \quad \text{where} \quad \hat{\gamma} = \sqrt{i \omega \mu \sigma - \omega^2 \mu \epsilon} \quad \text{(3 marks)}$$

- (iii) Set the propagation constant $\hat{\gamma} \equiv \alpha + i \beta$, to deduce that

$$\alpha = \frac{\omega \sqrt{\mu \epsilon}}{\sqrt{2}} \sqrt{\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} - 1} \quad . \quad \text{(6 marks)}$$

(Hint : $\sin\left(\frac{\theta}{2}\right) = \sqrt{\frac{1 - \cos(\theta)}{2}}$ & $\cos(\theta) = \left(\sqrt{1 + \tan^2(\theta)}\right)^{-1}$)

Question five

- (a) An uniform plane wave traveling along +z direction with the field components $E_x(z)$ & $H_y(z)$ has a complex electric field amplitude $\hat{E}_m^+ = 100 e^{i\frac{\pi}{6}} \frac{V}{m}$ and propagates at a frequency $f = 5 \times 10^7$ Hz in a material region has the parameters of $\mu = \mu_0$, $\epsilon = 2 \epsilon_0$ & $\frac{\sigma}{\omega \epsilon} = 0.3$.

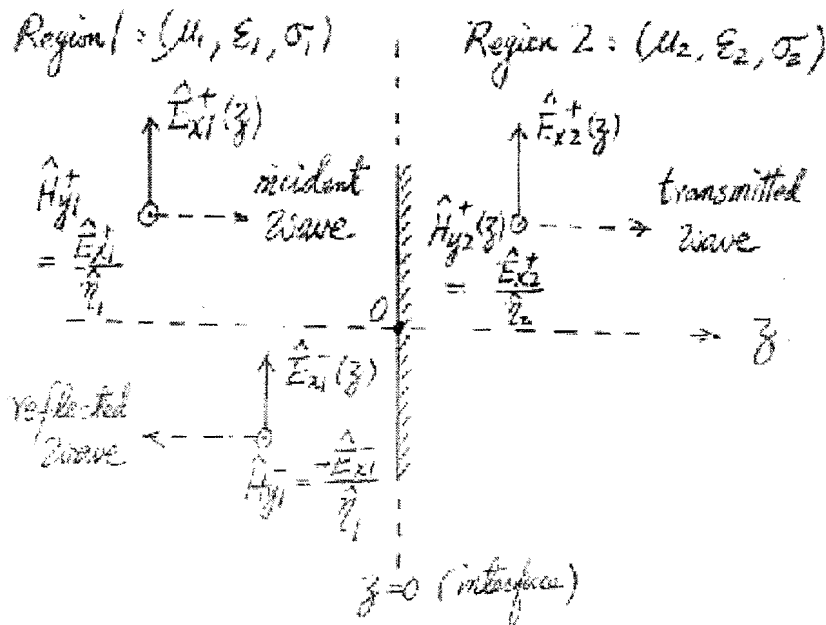
- (i) Find the values of the propagation constant $\hat{\gamma}$ ($= \alpha + i\beta$) and the intrinsic wave impedance $\hat{\eta}$ for this wave. (4 marks)
- (ii) Express the electric and magnetic fields in both their complex and real-time forms, with the numerical values of (a)(i) inserted. (4 marks)
- (iii) Find the values of the penetration depth, wave length and phase velocity of the given wave. (3 marks)

- (b) An uniform plane wave is incident normally upon an interface separating two regions.

The incident wave is given as $\left(\hat{E}_{x1}^+ = \hat{E}_{m1}^+ e^{-\hat{\gamma}_1 z}, \hat{H}_{y1}^+ = \frac{\hat{E}_{m1}^+}{\hat{\eta}_1} e^{-\hat{\gamma}_1 z} \right)$ and thus the

reflected and transmitted wave can be written as $\left(\hat{E}_{x1}^- = \hat{E}_{m1}^- e^{+\hat{\gamma}_1 z}, \hat{H}_{y1}^- = -\frac{\hat{E}_{m1}^-}{\hat{\eta}_1} e^{+\hat{\gamma}_1 z} \right)$

and $\left(\hat{E}_{x2}^+ = \hat{E}_{m2}^+ e^{-\hat{\gamma}_2 z}, \hat{H}_{y2}^+ = \frac{\hat{E}_{m2}^+}{\hat{\eta}_2} e^{-\hat{\gamma}_2 z} \right)$ respectively as shown below:



Question five (continued)

- (i) From the boundary conditions at the interface, i.e., both total \hat{E}_x & \hat{H}_y are continuous at $z = 0$, deduce the following

$$\begin{cases} \hat{E}_{m1}^- = \hat{E}_{m1}^+ \frac{\hat{\eta}_2 - \hat{\eta}_1}{\hat{\eta}_2 + \hat{\eta}_1} \\ \hat{E}_{m2}^+ = \hat{E}_{m1}^+ \frac{2\hat{\eta}_2}{\hat{\eta}_2 + \hat{\eta}_1} \end{cases} \quad (9 \text{ marks})$$

- (ii) If region 1 is air (i.e., $\hat{\eta}_1 = 120 \pi = 377 \ \Omega$), region 2 is a lossy medium with parameters of $\left(\mu_2 = \mu_0, \epsilon_2 = 9 \epsilon_0, \frac{\sigma_2}{\omega \epsilon_2} = 1 \right)$, and the incident plane wave is having a complex amplitude of $\hat{E}_{m1}^+ = 60 e^{i50^\circ} \frac{V}{m}$ and propagates at a frequency of $f = 10^6 \text{ Hz}$.

(A) Calculate the value of $\hat{\eta}_2$. (2 marks)

(B) Calculate the values of \hat{E}_{m2}^+ . (3 marks)

Useful informations

$$e = 1.6 \times 10^{-19} \text{ C}$$

$$m_e = 9.1 \times 10^{-31} \text{ kg}$$

$$\mu_0 = 4 \pi \times 10^{-7} \frac{\text{H}}{\text{m}}$$

$$\epsilon_0 = 8.85 \times 10^{-12} \frac{\text{F}}{\text{m}}$$

$$\alpha = \frac{\omega \sqrt{\mu \epsilon}}{\sqrt{2}} \sqrt{\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon}\right)^2} - 1}$$

$$\beta = \frac{\omega \sqrt{\mu \epsilon}}{\sqrt{2}} \sqrt{\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon}\right)^2} + 1}$$

$$\frac{1}{\sqrt{\mu_0 \epsilon_0}} = 3 \times 10^8 \frac{\text{m}}{\text{s}}$$

$$\hat{\eta} = \frac{\sqrt{\frac{\mu}{\epsilon}}}{\sqrt[4]{1 + \left(\frac{\sigma}{\omega \epsilon}\right)^2}} e^{i \frac{1}{2} \tan^{-1}\left(\frac{\sigma}{\omega \epsilon}\right)}$$

$$\eta_0 = 120 \pi \quad \Omega = 377 \quad \Omega$$

$$\beta_0 = \omega \sqrt{\mu_0 \epsilon_0}$$

$$\oiint_S \vec{E} \cdot d\vec{s} = \frac{1}{\epsilon} \iiint_V \rho_v \, dv$$

$$\oiint_S \vec{B} \cdot d\vec{s} = 0$$

$$\oint_L \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \left(\iint_S \vec{B} \cdot d\vec{s} \right)$$

$$\oint_L \vec{B} \cdot d\vec{l} = \mu \iint_S \vec{J} \cdot d\vec{s} + \mu \epsilon \frac{\partial}{\partial t} \left(\iint_S \vec{E} \cdot d\vec{s} \right)$$

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho_v}{\epsilon}$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{B} = \mu \vec{J} + \mu \epsilon \frac{\partial \vec{E}}{\partial t}$$

$$\vec{J} = \sigma \vec{E}$$

$$\iiint_S \vec{F} \cdot d\vec{s} \equiv \iiint_V (\vec{\nabla} \cdot \vec{F}) dV \quad \text{divergence theorem}$$

$$\oint_L \vec{F} \cdot d\vec{l} \equiv \iint_S (\vec{\nabla} \times \vec{F}) \cdot d\vec{s} \quad \text{Stokes' theorem}$$

$$\vec{\nabla} \cdot (\vec{\nabla} \times \vec{F}) \equiv 0$$

$$\vec{\nabla} \times (\vec{\nabla} f) \equiv 0$$

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{F}) \equiv \vec{\nabla} (\vec{\nabla} \cdot \vec{F}) - \nabla^2 \vec{F}$$

$$\begin{aligned} \vec{\nabla} f &= \vec{e}_x \frac{\partial f}{\partial x} + \vec{e}_y \frac{\partial f}{\partial y} + \vec{e}_z \frac{\partial f}{\partial z} = \vec{e}_\rho \frac{\partial f}{\partial \rho} + \vec{e}_\phi \frac{1}{\rho} \frac{\partial f}{\partial \phi} + \vec{e}_z \frac{\partial f}{\partial z} \\ &= \vec{e}_r \frac{\partial f}{\partial r} + \vec{e}_\theta \frac{1}{r} \frac{\partial f}{\partial \theta} + \vec{e}_\phi \frac{1}{r \sin(\theta)} \frac{\partial f}{\partial \phi} \end{aligned}$$

$$\begin{aligned} \vec{\nabla} \cdot \vec{F} &= \frac{\partial(F_x)}{\partial x} + \frac{\partial(F_y)}{\partial y} + \frac{\partial(F_z)}{\partial z} = \frac{1}{\rho} \frac{\partial(F_\rho \rho)}{\partial \rho} + \frac{1}{\rho} \frac{\partial(F_\phi)}{\partial \phi} + \frac{\partial(F_z)}{\partial z} \\ &= \frac{1}{r^2} \frac{\partial(F_r r^2)}{\partial r} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\theta \sin(\theta))}{\partial \theta} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\phi)}{\partial \phi} \end{aligned}$$

$$\begin{aligned} \vec{\nabla} \times \vec{F} &= \vec{e}_x \left(\frac{\partial(F_z)}{\partial y} - \frac{\partial(F_y)}{\partial z} \right) + \vec{e}_y \left(\frac{\partial(F_x)}{\partial z} - \frac{\partial(F_z)}{\partial x} \right) + \vec{e}_z \left(\frac{\partial(F_y)}{\partial x} - \frac{\partial(F_x)}{\partial y} \right) \\ &= \frac{\vec{e}_\rho}{\rho} \left(\frac{\partial(F_z)}{\partial \phi} - \frac{\partial(F_\phi \rho)}{\partial z} \right) + \vec{e}_\phi \left(\frac{\partial(F_\rho)}{\partial z} - \frac{\partial(F_z)}{\partial \rho} \right) + \frac{\vec{e}_z}{\rho} \left(\frac{\partial(F_\phi \rho)}{\partial \rho} - \frac{\partial(F_\rho)}{\partial \phi} \right) \\ &= \frac{\vec{e}_r}{r^2 \sin(\theta)} \left(\frac{\partial(F_\phi r \sin(\theta))}{\partial \theta} - \frac{\partial(F_\theta r)}{\partial \phi} \right) + \frac{\vec{e}_\theta}{r \sin(\theta)} \left(\frac{\partial(F_r)}{\partial \phi} - \frac{\partial(F_\phi r \sin(\theta))}{\partial r} \right) + \frac{\vec{e}_\phi}{r} \left(\frac{\partial(F_\theta r)}{\partial r} - \frac{\partial(F_r)}{\partial \theta} \right) \end{aligned}$$

where $\vec{F} = \vec{e}_x F_x + \vec{e}_y F_y + \vec{e}_z F_z = \vec{e}_\rho F_\rho + \vec{e}_\phi F_\phi + \vec{e}_z F_z = \vec{e}_r F_r + \vec{e}_\theta F_\theta + \vec{e}_\phi F_\phi$ and

$$d\vec{l} = \vec{e}_x dx + \vec{e}_y dy + \vec{e}_z dz = \vec{e}_\rho d\rho + \vec{e}_\phi \rho d\phi + \vec{e}_z dz = \vec{e}_r dr + \vec{e}_\theta r d\theta + \vec{e}_\phi r \sin(\theta) d\phi$$

$$\begin{aligned} \nabla^2 f &= \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2} = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\rho \frac{\partial f}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 f}{\partial \phi^2} + \frac{\partial^2 f}{\partial z^2} \\ &= \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial f}{\partial r} \right) + \frac{1}{r^2 \sin(\theta)} \frac{\partial}{\partial \theta} \left(\sin(\theta) \frac{\partial f}{\partial \theta} \right) + \frac{1}{r^2 \sin^2(\theta)} \frac{\partial^2 f}{\partial \phi^2} \end{aligned}$$