

**UNIVERSITY OF SWAZILAND**

**FACULTY OF SCIENCE AND ENGINEERING**

**DEPARTMENT OF PHYSICS**

**SUPPLEMENTARY EXAMINATION 2012/2013**

**TITLE OF PAPER : ELECTROMAGNETIC THEORY**

**COURSE NUMBER : P331**

**TIME ALLOWED : THREE HOURS**

**INSTRUCTIONS : ANSWER ANY FOUR OUT OF FIVE  
QUESTIONS.  
EACH QUESTION CARRIES 25 MARKS.**

**MARKS FOR DIFFERENT SECTIONS ARE  
SHOWN IN THE RIGHT-HAND MARGIN.**

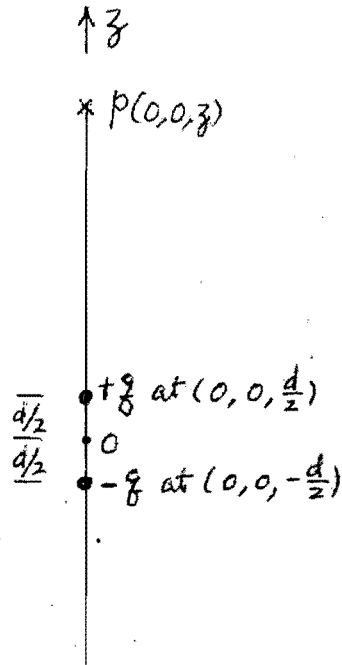
**THIS PAPER HAS TEN PAGES, INCLUDING THIS PAGE.**

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**P331 ELECTROMAGNETIC THEORY**

**Question one**

- (a) Two equal and opposite point charges  $\pm q$  which form an electric dipole with a dipole moment of  $\vec{p} = \vec{e}_z p = \vec{e}_z (q d)$ , situated at the origin is shown below.



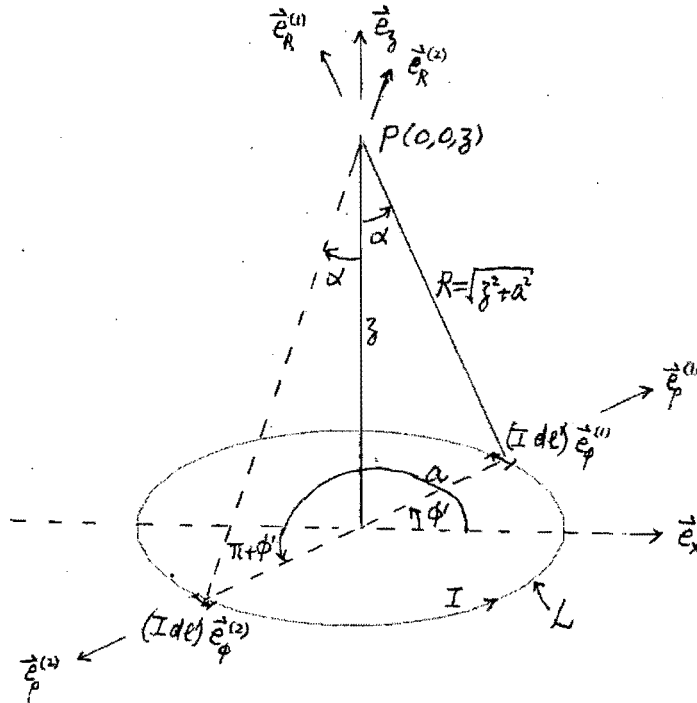
- (i) Use superposition principle to write down the electric scalar potential  $f$  at the field point  $P(0,0,z)$  due to those two point charges which form a dipole. Simplify it and deduce that

$$f = \frac{p}{4 \pi \epsilon_0 \left( z^2 - \left( \frac{d}{2} \right)^2 \right)} \quad (2 \text{ marks})$$

- (ii) Use  $\vec{E} \equiv -\vec{\nabla} f$  to find the electric field  $\vec{E}$  at the field point  $P(0,0,z)$  due to the given dipole. Then show that  $\vec{E} \approx \vec{e}_z \frac{p}{2 \pi \epsilon_0 z^3}$  if  $z \gg d$ . (6 marks)

**Question one (continued)**

- (b) A circular ring  $L$  of radius  $a$  carries a constant counter clockwise line current  $I$ . The ring is situated on  $z = 0$  plane with the ring's centre at the origin as shown in the following diagram



where  $\vec{e}_R^{(1)}$  &  $\vec{e}_R^{(2)}$  are the unit vectors pointing from the small line segment current sources  $(I dl) \vec{e}_\phi^{(1)}$  &  $(I dl) \vec{e}_\phi^{(2)}$  respectively to the field point  $P(0,0,z)$ .

- (i) Express  $\vec{e}_R^{(1)}$  &  $\vec{e}_R^{(2)}$  in terms of  $\vec{e}_\rho^{(1)}$ ;  $\vec{e}_\rho^{(2)}$ ;  $\vec{e}_z$  &  $\alpha$  and then show that  $\vec{e}_\phi^{(1)} \times \vec{e}_R^{(1)} + \vec{e}_\phi^{(2)} \times \vec{e}_R^{(2)} = \vec{e}_z 2 \cos(\alpha)$   
 (Hint :  $\vec{e}_\rho^{(1)} = -\vec{e}_\rho^{(2)}$  &  $\vec{e}_\phi^{(1)} = -\vec{e}_\phi^{(2)}$ ) ( 7 marks )

- (ii) From Biot-Savart law, i.e.,  $\vec{B} = \int_L \frac{\mu_0 (\vec{e}_\phi I dl) \times \vec{e}_R}{4 \pi R^2}$ , find the magnetic field  $\vec{B}$  at the field point  $P(0,0,z)$  produced by the given ring current source. ( 6 marks )

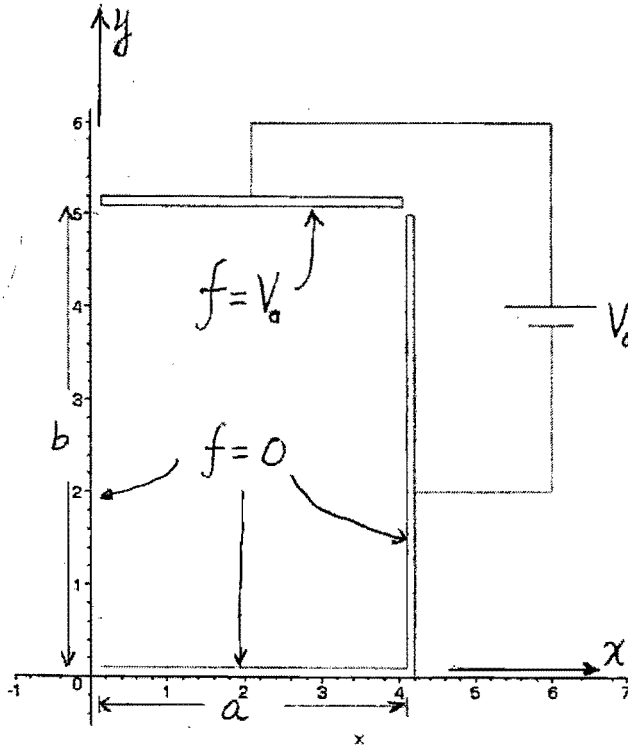
(Hint : use "pair" addition in (b)(i) and then integrate for half of the ring.)

- (iii) If  $z \gg a$ , find the approximate expression of  $\vec{B}$  from the result obtained in (b)(ii). Rewrite it in terms of magnetic dipole moment of the given current loop  $m$  where  $m \equiv I(\pi a^2)$  and compare it with the approximate expression of  $\vec{E}$  in (a)(ii).

Show that replacing  $\left( \frac{p}{\epsilon_0} \right)$  by  $(\mu_0 m)$  they are identical. ( 4 marks )

### Question two

A U – tube capacitor extended very long into z direction with its cross section as shown below :



Its electric potential  $f(x, y)$  in Cartesian coordinates for the region between two conductors, i.e.,  $0 \leq x \leq a$  &  $0 \leq y \leq b$ , satisfies the following two dimensional Laplace equation :

$$\frac{\partial^2 f(x, y)}{\partial x^2} + \frac{\partial^2 f(x, y)}{\partial y^2} = 0 .$$

- (a) Set  $f(x, y) = F(x) G(y)$  and use separation variable scheme  
 (i) to deduce the following two ordinary differential equations :

$$\begin{cases} \frac{d^2 F(x)}{dx^2} = k F(x) & \dots\dots (1) \\ \frac{d^2 G(y)}{dy^2} = -k G(y) & \dots\dots (2) \end{cases}$$

where  $k$  is the separation constant of any value. ( 4 marks )

- (ii) Based on the given initial conditions indicated in the above diagram, explain why only the negative values of  $k$  are desirable? Thus  $k$  can be written as  $-K^2$ .

( 3 marks )

- (iii) By direct substitution, show that  $A \cosh(K y) + B \sinh(K y)$ , where  $A$  &  $B$  are arbitrary constants, is a general solution to eq.(2) with  $k = -K^2$  where  $K$  is a positive constant and a better alternative for the separation constant. ( 3 marks )

**Question two (continued)**

(b) The general solution for (a) is

$$f(x, y) = \sum_{\forall K} f_K(x, y) \\ = \sum_{\forall K} (A_K \cos(Kx) + B_K \sin(Kx))(C_K \cosh(Ky) + D_K \sinh(Ky)) \dots\dots (3)$$

where  $A_K$ ,  $B_K$ ,  $C_K$  &  $D_K$  are arbitrary constants. This general solution is subjected to the following four boundary conditions :

$$BC(1) : f_K(0, y) = 0 \quad \forall \quad 0 \leq y \leq b$$

$$BC(2) : f_K(a, y) = 0 \quad \forall \quad 0 \leq y \leq b$$

$$BC(3) : f_K(x, 0) = 0 \quad \forall \quad 0 \leq x \leq a$$

$$BC(4) : f(x, b) = V_0 \quad \forall \quad 0 \leq x \leq a$$

(i) Apply BC(1) and deduce from eq.(3) that

$$f(x, y) = \sum_{\forall K} (B_K \sin(Kx))(C_K \cosh(Ky) + D_K \sinh(Ky)) \dots\dots (4)$$

**( 2 marks )**

(ii) Apply BC(3) and deduce from eq.(4) that

$$f(x, y) = \sum_{\forall K} (B_K \sin(Kx))(D_K \sinh(Ky)) \text{ name } (B_K D_K) \text{ as } E_K \\ = \sum_{\forall K} (E_K \sin(Kx) \sinh(Ky)) \dots\dots (5)$$

**( 2 marks )**

(iii) Apply BC(2) and deduce from eq.(5) that

$$f(x, y) = \sum_{n=1}^{\infty} \left( E_n \sin\left(\frac{n\pi x}{a}\right) \sinh\left(\frac{n\pi y}{a}\right) \right) \dots\dots (6) \quad \textbf{( 3 marks )}$$

(iv) Apply BC(4) and find the values of  $E_n$  in terms of  $V_0$ ,  $a$  &  $b$  and show that

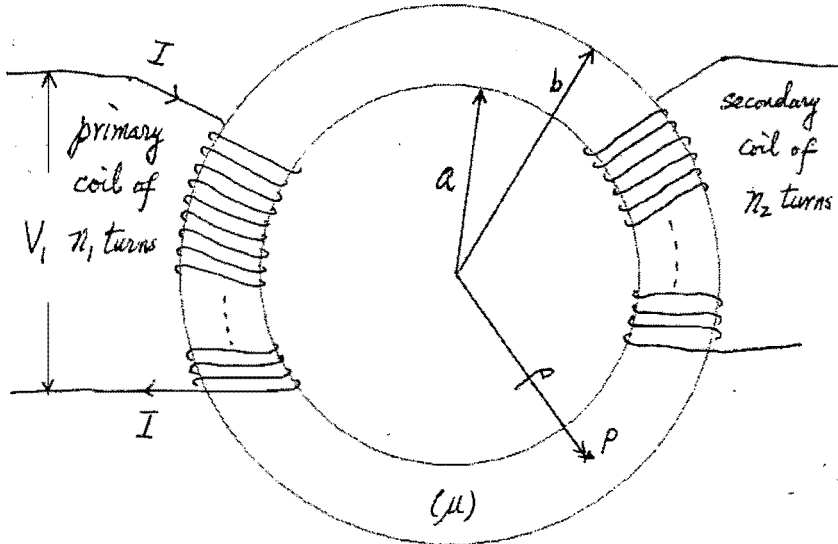
$$E_n = \frac{2 V_0 (1 - \cos(n\pi))}{n \pi \sinh\left(\frac{n\pi b}{a}\right)} \quad n = 1, 2, 3, \dots\dots \quad \text{. Also write down the specific}$$

solution to this given boundary value problem. **( 8 marks )**

$$\text{(Hint : } \int_{x=0}^a \sin\left(\frac{n\pi x}{a}\right) \sin\left(\frac{m\pi x}{a}\right) dx = \begin{cases} 0 & \text{if } n \neq m \\ \frac{a}{2} & \text{if } n = m \end{cases} \text{)}$$

### Question three

A static current  $I$  flows in the primary coil of  $n_1$  turn toroid, wired around an iron ring core of magnetic permeability  $\mu$  with the square cross-section area  $(b - a)^2$  as shown below:



- (a) Use the integral Ampere's law, choose and draw proper closed loops to find the magnetic field  $\vec{B}$  in terms of  $\rho$ ,  $n_1$ ,  $\mu$  &  $I$  within the iron core, i.e.,  $a \leq \rho \leq b$  &  $0 \leq z \leq (b - a)$  region. (1+6 marks)
- (b) Find the total magnetic flux  $\Psi_m$  passing through the cross-section area  $(b - a)^2$  of the iron ring in counter clockwise sense, i.e.,  $\int_S \vec{B} \cdot d\vec{s}$  where  $S: a \leq \rho \leq b$ ,  $0 \leq z \leq (b - a)$  &  $d\vec{s} = \vec{a}_\phi d\rho dz$ , in terms of  $a, b, n_1, \mu$  &  $I$ . (6 marks)
- (c) Find the self-inductance  $L$  of the primary coil as well as the mutual inductance  $M$  of the secondary coil due to the primary coil in terms of  $a, b, \mu, n_1$  &  $n_2$ . (5 marks)
- (d) (i) If the primary coil carries a sinusoidal current of  $I_0 \sin(\omega t)$  instead of carrying a static current  $I$ , find the induced e.m.f.  $V_2(t)$  for the secondary coil in terms of  $a, b, \omega, n_1, n_2, \mu$  &  $I_0$  under quasi static situation. (4 marks)
- (ii) If the potential drop for the primary coil due to its resistance is negligible compared to the one due to its self-inductance, i.e.,  $V_1(t) \approx L \frac{dI}{dt}$ , show that
- $$\frac{|V_2(t)|}{|V_1(t)|} = \frac{n_2}{n_1} . \quad \text{(3 marks)}$$

### Question four

(a) The Maxwell's equations for the empty space are

$$\vec{\nabla} \cdot \vec{E} = 0 \quad \dots\dots (1)$$

$$\vec{\nabla} \cdot \vec{B} = 0 \quad \dots\dots (2)$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \quad \dots\dots (3)$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t} \quad \dots\dots (4)$$

(i) Deduce from them the following wave equation for  $\vec{B}$  as

$$\nabla^2 \vec{B} = \mu_0 \epsilon_0 \frac{\partial^2 \vec{B}}{\partial t^2} \quad \dots\dots (5) \quad \text{( 4 marks )}$$

(ii) Given  $\vec{B} = \vec{e}_x B_m \cos(\omega t + \omega \sqrt{\mu_0 \epsilon_0} z + \phi)$ , where  $B_m$ ,  $\omega$  &  $\phi$  are constants,

(A) by direct substitution show that it is a solution to eq.(5) in (a)(i). ( 4 marks )

(B) setting its corresponding solution of  $\vec{E}$  as

$\vec{E} = \vec{e}_x E_x(z,t) + \vec{e}_y E_y(z,t) + \vec{e}_z E_z(z,t)$ , from eq.(3) deduce that

$$E_y(z,t) = \left( \frac{B_m}{\sqrt{\mu_0 \epsilon_0}} \right) \cos(\omega t + \omega \sqrt{\mu_0 \epsilon_0} z + \phi) \quad \text{( 6 marks )}$$

(b) An uniform plane wave traveling along +z direction with the field components

$\hat{E}_x(z)$  &  $\hat{H}_y(z)$  has a complex electric field amplitude  $\hat{E}_m^+ = 40 e^{i50^\circ} \frac{V}{m}$  and

propagates at a frequency  $f = 8 \times 10^6$  Hz in a material region having the parameters of

$$\mu = 8 \mu_0, \quad \epsilon = 2 \epsilon_0 \quad \& \quad \frac{\sigma}{\omega \epsilon} = 1.$$

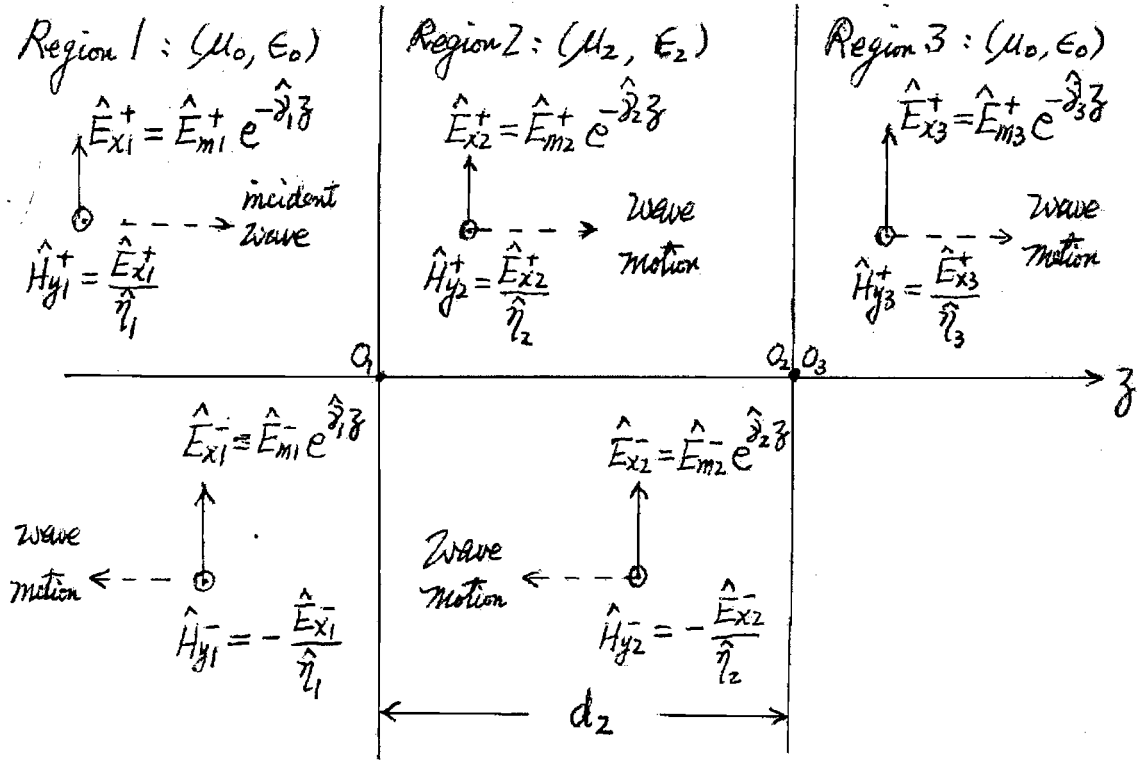
(i) Find the values of the propagation constant  $\hat{\gamma} (= \alpha + i \beta)$  and the intrinsic wave impedance  $\hat{\eta}$  for this wave. ( 4 marks )

(ii) Express the electric and magnetic fields in both their complex and real-time forms, with the numerical values of (a)(i) inserted. ( 4 marks )

(iii) Find the values of the penetration depth, wave length and phase velocity of the given wave. ( 3 marks )

### Question five

An uniform plane wave  $(\hat{E}_{x1}^+, \hat{H}_{y1}^+)$ , operating at  $f = 10^8$  Hz, is normally incident upon a lossless plate of quarter wavelength thickness, i.e.,  $d_2 = \frac{\lambda_2}{4}$ , with parameters of  $(\mu_2 = \mu_0, \epsilon_2 = 9\epsilon_0)$  as shown below :



$0_1$ ,  $0_2$  &  $0_3$  are the respective origins for region 1, 2 & 3 chosen at the first and second interface. (Both region 1 and region 3 are air regions.)

- (a) Define for the  $i^{\text{th}}$  region ( $i = 1, 2, 3$ ) the reflection coefficient  $\hat{\Gamma}_i(z)$  and the total wave impedance  $\hat{Z}_i(z)$  and deduce the following :

$$\hat{Z}_i(z) = \hat{\eta}_i \frac{1 + \hat{\Gamma}_i(z)}{1 - \hat{\Gamma}_i(z)} \quad (6 \text{ marks})$$

- (b) (i) Find the values of  $\hat{\gamma}_1$ ,  $\hat{\gamma}_2$ ,  $\hat{\gamma}_3$ ,  $\lambda_2$  &  $\hat{\eta}_2$ .  
(Note :  $\hat{\eta}_1 = \hat{\eta}_3 = 120 \pi \Omega$  and  $\alpha_1 = \alpha_2 = \alpha_3 = 0$ ) (4 marks)

- (ii) Starting with  $\hat{\Gamma}_3(z) = 0$  for the rightmost region, i.e., region 3, and using the boundary condition that  $\hat{Z}$  is continuous at the interface, find the values of  $\hat{Z}_3(0)$ ,  $\hat{Z}_2(0)$ ,  $\hat{\Gamma}_2(0)$ ,  $\hat{\Gamma}_2(-d_2)$ ,  $\hat{Z}_2(-d_2)$ ,  $\hat{Z}_1(0)$  &  $\hat{\Gamma}_1(0)$ . (9 marks)

- (iii) Find the value of  $\hat{E}_{m1}^-$  &  $\hat{E}_{m2}^+$  if given  $\hat{E}_{m1}^+ = 80 e^{i0} \frac{V}{m}$ . (6 marks)



### Useful informations

$$e = 1.6 \times 10^{-19} \text{ C}$$

$$m_e = 9.1 \times 10^{-31} \text{ kg}$$

$$\mu_0 = 4 \pi \times 10^{-7} \frac{\text{H}}{\text{m}}$$

$$\varepsilon_0 = 8.85 \times 10^{-12} \frac{\text{F}}{\text{m}}$$

$$\alpha = \frac{\omega \sqrt{\mu \varepsilon}}{\sqrt{2}} \sqrt{\sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} - 1}$$

$$\beta = \frac{\omega \sqrt{\mu \varepsilon}}{\sqrt{2}} \sqrt{\sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} + 1}$$

$$\frac{1}{\sqrt{\mu_0 \varepsilon_0}} = 3 \times 10^8 \frac{\text{m}}{\text{s}}$$

$$\hat{\eta} = \frac{\sqrt{\frac{\mu}{\varepsilon}}}{\sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2}} e^{i \frac{1}{2} \tan^{-1}\left(\frac{\sigma}{\omega \varepsilon}\right)}$$

$$\eta_0 = 120 \pi \quad \Omega = 377 \quad \Omega$$

$$\beta_0 = \omega \sqrt{\mu_0 \varepsilon_0}$$

$$\oiint_S \vec{E} \cdot d\vec{s} = \frac{1}{\varepsilon} \iiint_V \rho_v \, dv$$

$$\oiint_S \vec{B} \cdot d\vec{s} = 0$$

$$\oint_L \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \left( \iint_S \vec{B} \cdot d\vec{s} \right)$$

$$\oint_L \vec{B} \cdot d\vec{l} = \mu \iint_S \vec{J} \cdot d\vec{s} + \mu \varepsilon \frac{\partial}{\partial t} \left( \iint_S \vec{E} \cdot d\vec{s} \right)$$

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho_v}{\varepsilon}$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{B} = \mu \vec{J} + \mu \varepsilon \frac{\partial \vec{E}}{\partial t}$$

$$\vec{J} = \sigma \vec{E}$$

$$\oiint_S \vec{F} \cdot d\vec{s} \equiv \iiint_V (\vec{\nabla} \cdot \vec{F}) dV \quad \text{divergence theorem}$$

$$\oint_L \vec{F} \cdot d\vec{l} \equiv \iint_S (\vec{\nabla} \times \vec{F}) \cdot d\vec{s} \quad \text{Stokes' theorem}$$

$$\vec{\nabla} \cdot (\vec{\nabla} \times \vec{F}) \equiv 0$$

$$\vec{\nabla} \times (\vec{\nabla} f) \equiv 0$$

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{F}) \equiv \vec{\nabla} (\vec{\nabla} \cdot \vec{F}) - \nabla^2 \vec{F}$$

$$\vec{\nabla} f = \vec{e}_x \frac{\partial f}{\partial x} + \vec{e}_y \frac{\partial f}{\partial y} + \vec{e}_z \frac{\partial f}{\partial z} = \vec{e}_\rho \frac{\partial f}{\partial \rho} + \vec{e}_\phi \frac{1}{\rho} \frac{\partial f}{\partial \phi} + \vec{e}_z \frac{\partial f}{\partial z}$$

$$= \vec{e}_r \frac{\partial f}{\partial r} + \vec{e}_\theta \frac{1}{r} \frac{\partial f}{\partial \theta} + \vec{e}_\phi \frac{1}{r \sin(\theta)} \frac{\partial f}{\partial \phi}$$

$$\vec{\nabla} \cdot \vec{F} = \frac{\partial(F_x)}{\partial x} + \frac{\partial(F_y)}{\partial y} + \frac{\partial(F_z)}{\partial z} = \frac{1}{\rho} \frac{\partial(F_\rho \rho)}{\partial \rho} + \frac{1}{\rho} \frac{\partial(F_\phi)}{\partial \phi} + \frac{\partial(F_z)}{\partial z}$$

$$= \frac{1}{r^2} \frac{\partial(F_r r^2)}{\partial r} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\theta \sin(\theta))}{\partial \theta} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\phi)}{\partial \phi}$$

$$\vec{\nabla} \times \vec{F} = \vec{e}_x \left( \frac{\partial(F_z)}{\partial y} - \frac{\partial(F_y)}{\partial z} \right) + \vec{e}_y \left( \frac{\partial(F_x)}{\partial z} - \frac{\partial(F_z)}{\partial x} \right) + \vec{e}_z \left( \frac{\partial(F_y)}{\partial x} - \frac{\partial(F_x)}{\partial y} \right)$$

$$= \frac{\vec{e}_\rho}{\rho} \left( \frac{\partial(F_z)}{\partial \phi} - \frac{\partial(F_\phi \rho)}{\partial z} \right) + \vec{e}_\phi \left( \frac{\partial(F_\rho)}{\partial z} - \frac{\partial(F_z)}{\partial \rho} \right) + \frac{\vec{e}_z}{\rho} \left( \frac{\partial(F_\phi \rho)}{\partial \rho} - \frac{\partial(F_\rho)}{\partial \phi} \right)$$

$$= \frac{\vec{e}_r}{r^2 \sin(\theta)} \left( \frac{\partial(F_\phi r \sin(\theta))}{\partial \theta} - \frac{\partial(F_\theta r)}{\partial \phi} \right) + \frac{\vec{e}_\theta}{r \sin(\theta)} \left( \frac{\partial(F_r)}{\partial \phi} - \frac{\partial(F_\phi r \sin(\theta))}{\partial r} \right) + \frac{\vec{e}_\phi}{r} \left( \frac{\partial(F_\theta r)}{\partial r} - \frac{\partial(F_r)}{\partial \theta} \right)$$

where  $\vec{F} = \vec{e}_x F_x + \vec{e}_y F_y + \vec{e}_z F_z = \vec{e}_\rho F_\rho + \vec{e}_\phi F_\phi + \vec{e}_z F_z = \vec{e}_r F_r + \vec{e}_\theta F_\theta + \vec{e}_\phi F_\phi$  and

$$d\vec{l} = \vec{e}_x dx + \vec{e}_y dy + \vec{e}_z dz = \vec{e}_\rho d\rho + \vec{e}_\phi \rho d\phi + \vec{e}_z dz = \vec{e}_r dr + \vec{e}_\theta r d\theta + \vec{e}_\phi r \sin(\theta) d\phi$$

$$\nabla^2 f = \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2} = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left( \rho \frac{\partial f}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 f}{\partial \phi^2} + \frac{\partial^2 f}{\partial z^2}$$

$$= \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial f}{\partial r} \right) + \frac{1}{r^2 \sin(\theta)} \frac{\partial}{\partial \theta} \left( \sin(\theta) \frac{\partial f}{\partial \theta} \right) + \frac{1}{r^2 \sin^2(\theta)} \frac{\partial^2 f}{\partial \phi^2}$$

$$\hat{Z}_i(z) = \hat{\eta}_i \frac{1 + \hat{\Gamma}_i(z)}{1 - \hat{\Gamma}_i(z)}, \quad \hat{\Gamma}_i(z) = \frac{\hat{Z}_i(z) - \hat{\eta}_i}{\hat{Z}_i(z) + \hat{\eta}_i} \quad \&$$

$$\hat{\Gamma}_i(z') = \hat{\Gamma}_i(z) e^{2\hat{\eta}_i(z'-z)} \quad \text{where } z' \text{ \& } z \text{ are two points in } i^{\text{th}} \text{ region}$$