

**UNIVERSITY OF SWAZILAND**

149

**FACULTY OF SCIENCE AND ENGINEERING**

**DEPARTMENT OF PHYSICS**

**SUPPLEMENTARY EXAMINATION 2013/2014**

**TITLE OF PAPER : ELECTROMAGNETIC THEORY**

**COURSE NUMBER : P331**

**TIME ALLOWED : THREE HOURS**

**INSTRUCTIONS : ANSWER ANY FOUR OUT OF FIVE  
QUESTIONS.  
EACH QUESTION CARRIES 25 MARKS.**

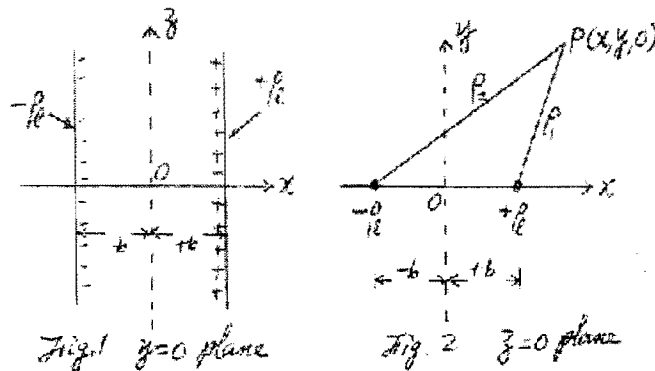
**MARKS FOR DIFFERENT SECTIONS ARE  
SHOWN IN THE RIGHT-HAND MARGIN.**

**THIS PAPER HAS EIGHT PAGES, INCLUDING THIS PAGE.**

**DO NOT OPEN THE PAPER UNTIL PERMISSION HAS BEEN  
GIVEN BY THE INVIGILATOR.**

Question one

- (a) A very long thin conducting wire situated at z-axis and uniformly charged with line charge density  $\rho_l$ ,
- (i) use integral electric Gauss Law and draw an appropriate Gaussian surface, deduce that the electric field at a field point outside the given thin conducting wire is
- $$\vec{E} = \vec{e}_\rho \frac{\rho_l}{2\pi\epsilon_0\rho}$$
- where  $\rho$  is the distance from z-axis and  $\vec{e}_\rho$  is one of the unit vectors in cylindrical coordinate system (2 + 6 marks)
- (ii) use  $\Phi = - \int_{P_0}^P \vec{E} \cdot d\vec{l}$  to find the electric potential at point P where  $P_0$  is the zero potential reference point here taken as  $P_0 : (\rho_0, 0, 0)$ , deduce that
- $$\Phi = \frac{\rho_l}{2\pi\epsilon_0} \ln\left(\frac{\rho_0}{\rho}\right)$$
- (4 marks)
- (b) Two long thin conducting wires parallel to z-axis and lying on the  $y = 0$  plane, i.e.  $x-z$  plane, one situated at  $x = -b$  and carries  $-\rho_l$  uniform line charge density and the other situated at  $x = +b$  and carries  $+\rho_l$  uniform line charge density as shown in the Figure.1 (on  $y = 0$  plane) and Figure.2 (on  $z = 0$  plane) below :

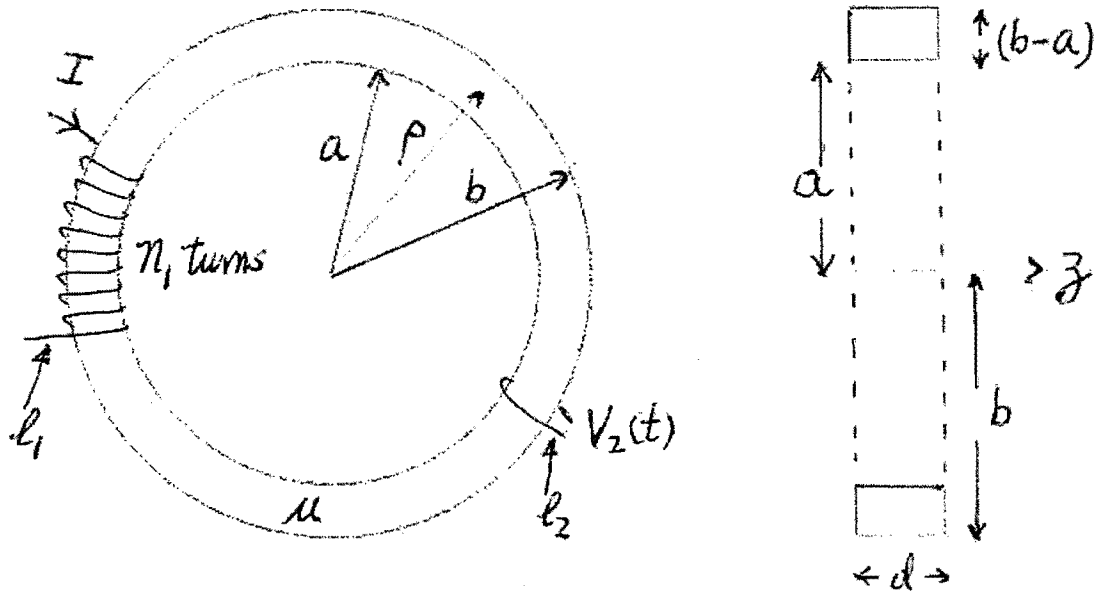


- (i) Utilize the result in (a)(ii) and choose  $P_0$  as the origin, apply the superposition principle to deduce that the electric potential at point  $P : (x, y, 0)$  is
- $$\Phi = \frac{\rho_l}{4\pi\epsilon_0} \ln\left(\frac{(x+b)^2 + y^2}{(x-b)^2 + y^2}\right)$$
- (6 marks)
- (ii) Set  $\frac{(x+b)^2 + y^2}{(x-b)^2 + y^2} = K$  where  $K$  is a positive constant thus implies  $\Phi$  is a constant, rewrite it to become a standard form of a circle and show that an equal potential surface is centred at  $\left(x_0 = b \frac{K+1}{K-1}, y_0 = 0\right)$  with a radius of  $R = \frac{2\sqrt{K}b}{|K-1|}$ . Discuss briefly the limiting cases when  $K \rightarrow 0^+$  &  $K \rightarrow +\infty$ . (5 + 2 marks)

**Question two**

146

- (a) A steady current  $I$  flows in the  $n_1$  ( $\gg 1$ ) turns coil  $l_1$  wiring around an iron ring core of magnetic permeability  $\mu$  ( $\gg \mu_0$ ) with the rectangular cross-section area  $(b-a) \times d$  as shown below



- (i) Set  $\vec{H}(\rho, \phi, z) = \vec{e}_\phi H_\phi(\rho)$  (write a brief justification for this setting), draw an appropriate closed loop  $L$  and utilize the integral form of Ampere's law, i.e.,  $\oint_L \vec{H} \cdot d\vec{l} = \{total\ I\ pass\ through\ S\ bounded\ by\ L\}$ , to find  $H_\phi(\rho)$  for  $a < \rho < b$  region. Then write down the magnetic field  $\vec{B}$  for  $a < \rho < b$  region. **(2 + 2 + 5 marks)**
- (ii) Find the total magnetic flux  $\Psi_m$  passing through the cross-section area  $(b-a) \times d$  of the iron ring in counter clockwise sense, i.e.,  $\int_S \vec{B} \cdot d\vec{s}$  where  $S: a \leq \rho \leq b, 0 \leq z \leq d$  &  $d\vec{s} = \vec{a}_\phi d\rho dz$ , in terms of  $a, b, d, n_1, \mu$  &  $I$ . **(4 marks)**
- (iii) Find the external self-inductance  $L_e$  of  $l_1$  coil and the mutual inductance  $M$  between  $l_1$  &  $l_2$  coils where  $l_2$  is a single turn secondary coil. **(5 marks)**
- (b) If  $l_1$  coil carries a sinusoidal current of  $I_0 \sin(\omega t)$  instead of carrying a steady current  $I$ , find the induced e.m.f.  $V_2(t)$  for a single turn secondary coil  $l_2$  in terms of  $a, b, d, \omega, n_1, \mu$  &  $I_0$  under quasi static situation. If  $a = 5\ cm, b = 6\ cm, d = 2\ cm, n_1 = 100, f = 100\ Hz, \mu = 100\ \mu_0$  and  $I_0 = 3\ A$ , compute the amplitude of  $V_2(t)$ . **(3 + 4 marks)**

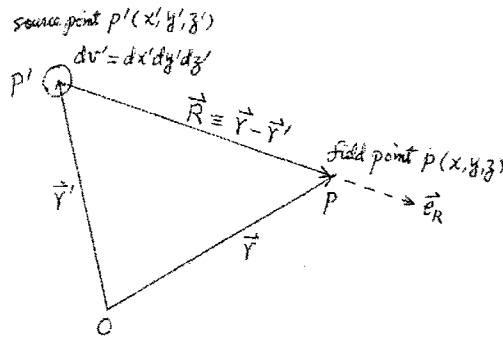
(a) The integral form of equation of continuity in Electromagnetic theory is

$$\oiint_S \vec{J} \cdot d\vec{s} = -\frac{\partial}{\partial t} \left( \iiint_V \rho_v dV \right) \text{ where } V \text{ is enclosed by closed surface } S$$

- (i) Explain briefly each term of the above equation and indicate which law of Physics it describes. (3 marks)
- (ii) Utilize the Divergence theory to convert the above integral equation into the differential form of equation of continuity. (3 marks)
- (iii) Which term in the differential form of Maxwell's equations is the "displacement current" term? Explain in details why Maxwell deemed it necessary to include this "extra" term in Maxwell's equations. (1 + 6 marks)

(b) According to Coulomb's law, the electric field  $\vec{E}$  at a field point  $\vec{r}$  produced by a tiny charge  $\rho_v(\vec{r}') dV'$  at a source point  $\vec{r}'$  is  $\vec{E}(\vec{r}) = \vec{e}_R \frac{\rho_v(\vec{r}') dV'}{4\pi\epsilon R^2}$  where  $\vec{r}$ ,  $\vec{r}'$  &  $\vec{e}_R$

are shown in the figure below :



From the superposition principle the electric field  $\vec{E}$  at a field point  $\vec{r}$  produced by all the electric charges is  $\vec{E}(\vec{r}) = \iiint_{V'} \vec{e}_R \frac{\rho_v(\vec{r}') dV'}{4\pi\epsilon R^2}$  ..... (1)

(i) By direct differentiation, show that  $\vec{\nabla} \left( \frac{1}{R} \right) = -\vec{e}_R \frac{1}{R^2}$  where gradient operator  $\vec{\nabla}$  is operating on field point  $(x, y, z)$ . (7 marks)

(Note:  $\vec{r} = \vec{e}_x x + \vec{e}_y y + \vec{e}_z z$ ,  $\vec{r}' = \vec{e}_x x' + \vec{e}_y y' + \vec{e}_z z'$  &  $\vec{R} \equiv \vec{r} - \vec{r}' = \vec{e}_x (x - x') + \vec{e}_y (y - y') + \vec{e}_z (z - z') = \vec{e}_R R$  where

$$\left[ \begin{aligned} R &= \sqrt{(x - x')^2 + (y - y')^2 + (z - z')^2} \\ \vec{e}_R &= \vec{e}_x \frac{(x - x')}{R} + \vec{e}_y \frac{(y - y')}{R} + \vec{e}_z \frac{(z - z')}{R} \end{aligned} \right)$$

(ii) Take the minus gradient of  $f(\vec{r}) = \iiint_{V'} \frac{\rho_v(\vec{r}') dV'}{4\pi\epsilon_0 R}$  and use the results of (b)(i) and eq.(1) to deduce that  $\vec{E}(\vec{r}) \equiv -\vec{\nabla} (f(\vec{r}))$ . (5 marks)

Question four

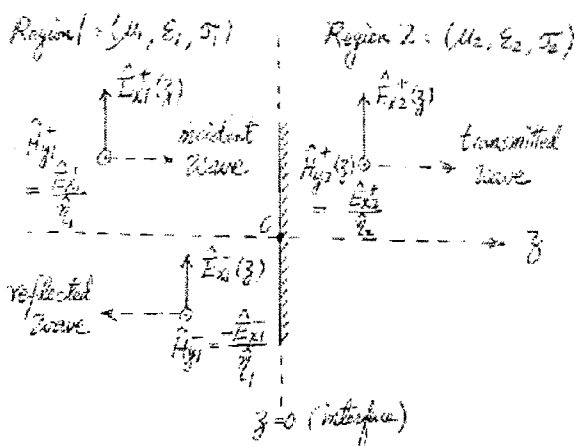
148

An uniform plane wave is normally incident upon an interface separating two regions as shown

below. The incident wave is given as  $\left( \hat{E}_{x1}^+ = \hat{E}_{m1}^+ e^{-\hat{\eta}_1 z}, \hat{H}_{y1}^+ = \frac{\hat{E}_{m1}^+}{\hat{\eta}_1} e^{-\hat{\eta}_1 z} \right)$  and thus the

reflected and transmitted wave can be written as  $\left( \hat{E}_{x1}^- = \hat{E}_{m1}^- e^{+\hat{\eta}_1 z}, \hat{H}_{y1}^- = -\frac{\hat{E}_{m1}^-}{\hat{\eta}_1} e^{+\hat{\eta}_1 z} \right)$  and

$\left( \hat{E}_{x2}^+ = \hat{E}_{m2}^+ e^{-\hat{\eta}_2 z}, \hat{H}_{y2}^+ = \frac{\hat{E}_{m2}^+}{\hat{\eta}_2} e^{-\hat{\eta}_2 z} \right)$  respectively as shown in the figure below:



- (a) From the boundary conditions at the interface, i.e., both total  $\hat{E}_x$  &  $\hat{H}_y$  are continuous at  $z = 0$ , deduce the following

$$\begin{cases} \hat{E}_{m1}^- = \hat{E}_{m1}^+ \frac{\hat{\eta}_2 - \hat{\eta}_1}{\hat{\eta}_2 + \hat{\eta}_1} \\ \hat{E}_{m2}^+ = \hat{E}_{m1}^+ \frac{2\hat{\eta}_2}{\hat{\eta}_2 + \hat{\eta}_1} \end{cases} \quad (11 \text{ marks})$$

- (b) If given  $\hat{E}_{m1}^+ = 100 e^{i0^\circ} \frac{V}{m}$ ,  $f = 10^6 \text{ Hz}$ , region 1 is having parameters of

$$\left( \mu_1 = \mu_0, \epsilon_1 = 4\epsilon_0 \text{ \& } \frac{\sigma_1}{\omega\epsilon_1} = 0.5 \right) \text{ and region 2 is having parameters of}$$

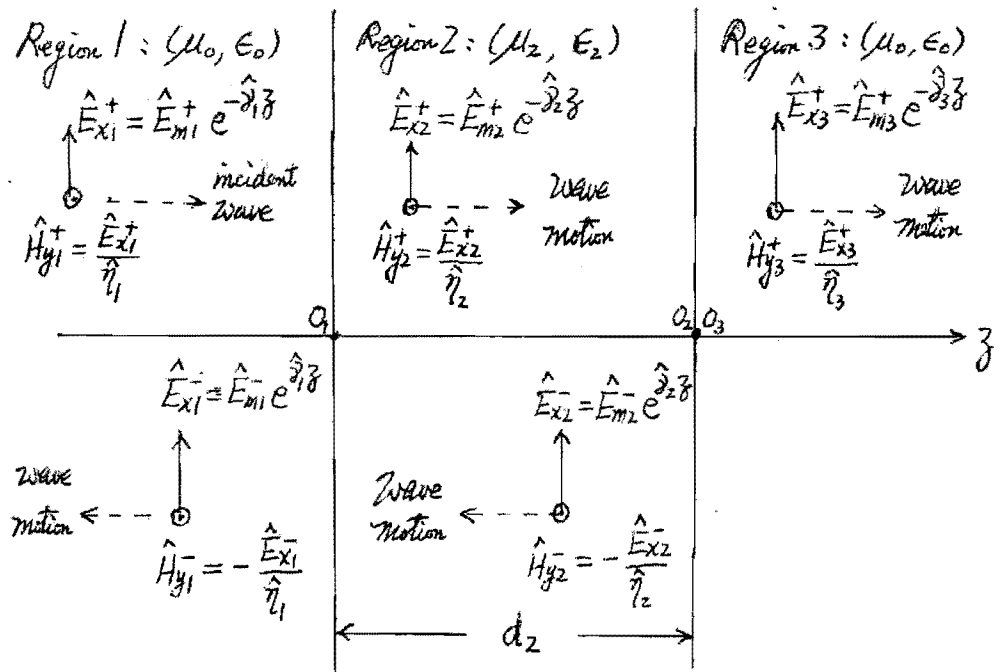
$$\left( \mu_2 = \mu_0, \epsilon_2 = 9\epsilon_0 \text{ \& } \frac{\sigma_2}{\omega\epsilon_2} = 1 \right),$$

- (i) Find the values of  $\hat{\eta}_1$  &  $\hat{\eta}_2$ . (4 marks)
- (ii) Find the values of  $\hat{E}_{m1}^-$  &  $\hat{E}_{m2}^+$  and express them in polar form. (7 marks)
- (iii) What would be the values of  $\hat{E}_{m1}^-$  &  $\hat{E}_{m2}^+$  approaching to if the region 2 is a very good conductive region? (3 marks)

Question five

149

An uniform plane wave  $(\hat{E}_{x1}^+, \hat{H}_{y1}^+)$ , operates at  $f = 10^7$  Hz, is normally incident upon a lossless layer of quarter wave thickness  $d_2 = \frac{\lambda_2}{4}$  with parameters of  $(\mu_2 = \mu_0, \epsilon_2 = 16 \epsilon_0)$  as shown below :



$0_1, 0_2$  &  $0_3$  are the respective origins for region 1, 2 & 3 chosen at the first and second interface. (Both region 1 and region 3 are air region.)

(a) Find the values of  $\beta_0, \hat{\gamma}_2 (= \alpha_2 + j\beta_2)$  &  $\hat{\eta}_2$ . (5 marks)

(Note:  $\hat{\gamma}_1 = \hat{\gamma}_3 = j\beta_0 = j\omega\sqrt{\mu_0\epsilon_0}$  &  $\hat{\eta}_1 = \hat{\eta}_3 = 377 = 120\pi$ )

(b) Find all the  $\hat{Z}$  &  $\hat{\Gamma}$  values at two interfaces, i.e.,  $\hat{\Gamma}_3(0_3), \hat{Z}_3(0_3), \hat{Z}_2(0_2), \hat{\Gamma}_2(0_2), \hat{\Gamma}_2(-d_2), \hat{Z}_2(-d_2), \hat{Z}_1(0_1)$  &  $\hat{\Gamma}_1(0_1)$  (10 marks)

(c) Find the values of  $\hat{E}_{m1}^-, \hat{E}_{m2}^+, \hat{E}_{m2}^-$  &  $\hat{E}_{m3}^+$  if given  $\hat{E}_{m1}^+ = 100 e^{j0}$   $\frac{V}{m}$  (10 marks)

$$e = 1.6 \times 10^{-19} \text{ C}$$

$$m_e = 9.1 \times 10^{-31} \text{ kg}$$

$$\mu_0 = 4 \pi \times 10^{-7} \frac{\text{H}}{\text{m}}$$

$$\varepsilon_0 = 8.85 \times 10^{-12} \frac{\text{F}}{\text{m}}$$

$$\alpha = \frac{\omega \sqrt{\mu \varepsilon}}{\sqrt{2}} \sqrt{\sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} - 1}$$

$$\beta = \frac{\omega \sqrt{\mu \varepsilon}}{\sqrt{2}} \sqrt{\sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} + 1}$$

$$\frac{1}{\sqrt{\mu_0 \varepsilon_0}} = 3 \times 10^8 \frac{\text{m}}{\text{s}}$$

$$\hat{\eta} = \frac{\sqrt{\frac{\mu}{\varepsilon}}}{\sqrt[4]{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2}} e^{i \frac{1}{2} \tan^{-1}\left(\frac{\sigma}{\omega \varepsilon}\right)}$$

$$\eta_0 = \sqrt{\frac{\mu_0}{\varepsilon_0}} = 120 \pi \quad \Omega = 377 \quad \Omega$$

$$\beta_0 = \omega \sqrt{\mu_0 \varepsilon_0}$$

$$\oiint_S \vec{E} \cdot d\vec{s} = \frac{1}{\varepsilon} \iiint_V \rho_v \, dv$$

$$\oiint_S \vec{B} \cdot d\vec{s} \equiv 0$$

$$\oint_L \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \left( \iint_S \vec{B} \cdot d\vec{s} \right)$$

$$\oint_L \vec{B} \cdot d\vec{l} = \mu \iint_S \vec{J} \cdot d\vec{s} + \mu \varepsilon \frac{\partial}{\partial t} \left( \iint_S \vec{E} \cdot d\vec{s} \right)$$

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho_v}{\varepsilon}$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{B} = \mu \vec{J} + \mu \varepsilon \frac{\partial \vec{E}}{\partial t}$$

$$\vec{J} = \sigma \vec{E}$$

$$\vec{D} = \epsilon \vec{E} = \epsilon_0 \vec{E} + \vec{P} \quad \& \quad \vec{B} = \mu \vec{H} = \mu_0 \vec{H} + \vec{M} \quad (5)$$

$$\oiint_S \vec{F} \cdot d\vec{s} \equiv \iiint_V (\vec{\nabla} \cdot \vec{F}) dV \quad \text{divergence theorem}$$

$$\oint_L \vec{F} \cdot d\vec{l} \equiv \iint_S (\vec{\nabla} \times \vec{F}) \cdot d\vec{s} \quad \text{Stokes' theorem}$$

$$\vec{\nabla} \cdot (\vec{\nabla} \times \vec{F}) \equiv 0$$

$$\vec{\nabla} \times (\vec{\nabla} f) \equiv 0$$

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{F}) \equiv \vec{\nabla} (\vec{\nabla} \cdot \vec{F}) - \nabla^2 \vec{F}$$

$$\begin{aligned} \vec{\nabla} f &= \vec{e}_x \frac{\partial f}{\partial x} + \vec{e}_y \frac{\partial f}{\partial y} + \vec{e}_z \frac{\partial f}{\partial z} = \vec{e}_\rho \frac{\partial f}{\partial \rho} + \vec{e}_\phi \frac{1}{\rho} \frac{\partial f}{\partial \phi} + \vec{e}_z \frac{\partial f}{\partial z} \\ &= \vec{e}_r \frac{\partial f}{\partial r} + \vec{e}_\theta \frac{1}{r} \frac{\partial f}{\partial \theta} + \vec{e}_\phi \frac{1}{r \sin(\theta)} \frac{\partial f}{\partial \phi} \end{aligned}$$

$$\begin{aligned} \vec{\nabla} \cdot \vec{F} &= \frac{\partial(F_x)}{\partial x} + \frac{\partial(F_y)}{\partial y} + \frac{\partial(F_z)}{\partial z} = \frac{1}{\rho} \frac{\partial(F_\rho \rho)}{\partial \rho} + \frac{1}{\rho} \frac{\partial(F_\phi)}{\partial \phi} + \frac{\partial(F_z)}{\partial z} \\ &= \frac{1}{r^2} \frac{\partial(F_r r^2)}{\partial r} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\theta \sin(\theta))}{\partial \theta} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\phi)}{\partial \phi} \end{aligned}$$

$$\begin{aligned} \vec{\nabla} \times \vec{F} &= \vec{e}_x \left( \frac{\partial(F_z)}{\partial y} - \frac{\partial(F_y)}{\partial z} \right) + \vec{e}_y \left( \frac{\partial(F_x)}{\partial z} - \frac{\partial(F_z)}{\partial x} \right) + \vec{e}_z \left( \frac{\partial(F_y)}{\partial x} - \frac{\partial(F_x)}{\partial y} \right) \\ &= \frac{\vec{e}_\rho}{\rho} \left( \frac{\partial(F_z)}{\partial \phi} - \frac{\partial(F_\phi \rho)}{\partial z} \right) + \vec{e}_\phi \left( \frac{\partial(F_\rho)}{\partial z} - \frac{\partial(F_z)}{\partial \rho} \right) + \frac{\vec{e}_z}{\rho} \left( \frac{\partial(F_\phi \rho)}{\partial \rho} - \frac{\partial(F_\rho)}{\partial \phi} \right) \\ &= \frac{\vec{e}_r}{r^2 \sin(\theta)} \left( \frac{\partial(F_\phi r \sin(\theta))}{\partial \theta} - \frac{\partial(F_\theta r)}{\partial \phi} \right) + \frac{\vec{e}_\theta}{r \sin(\theta)} \left( \frac{\partial(F_r)}{\partial \phi} - \frac{\partial(F_\phi r \sin(\theta))}{\partial r} \right) + \frac{\vec{e}_\phi}{r} \left( \frac{\partial(F_\theta r)}{\partial r} - \frac{\partial(F_r)}{\partial \theta} \right) \end{aligned}$$

where  $\vec{F} = \vec{e}_x F_x + \vec{e}_y F_y + \vec{e}_z F_z = \vec{e}_\rho F_\rho + \vec{e}_\phi F_\phi + \vec{e}_z F_z = \vec{e}_r F_r + \vec{e}_\theta F_\theta + \vec{e}_\phi F_\phi$  and

$$d\vec{l} = \vec{e}_x dx + \vec{e}_y dy + \vec{e}_z dz = \vec{e}_\rho d\rho + \vec{e}_\phi \rho d\phi + \vec{e}_z dz = \vec{e}_r dr + \vec{e}_\theta r d\theta + \vec{e}_\phi r \sin(\theta) d\phi$$

$$\begin{aligned} \nabla^2 f &= \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2} = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left( \rho \frac{\partial f}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 f}{\partial \phi^2} + \frac{\partial^2 f}{\partial z^2} \\ &= \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial f}{\partial r} \right) + \frac{1}{r^2 \sin(\theta)} \frac{\partial}{\partial \theta} \left( \sin(\theta) \frac{\partial f}{\partial \theta} \right) + \frac{1}{r^2 \sin^2(\theta)} \frac{\partial^2 f}{\partial \phi^2} \end{aligned}$$

$$\hat{Z}_i(z) = \hat{\eta}_i \frac{1 + \hat{\Gamma}_i(z)}{1 - \hat{\Gamma}_i(z)} \quad , \quad \hat{\Gamma}_i(z) = \frac{\hat{Z}_i(z) - \hat{\eta}_i}{\hat{Z}_i(z) + \hat{\eta}_i} \quad \&$$

$$\hat{\Gamma}_i(z') = \hat{\Gamma}_i(z) e^{2\hat{\eta}_i(z' - z)} \quad \text{where } z' \text{ \& } z \text{ are two positions in } i^{\text{th}} \text{ region}$$