

UNIVERSITY OF SWAZILAND

103

FACULTY OF SCIENCE AND ENGINEERING

DEPARTMENT OF PHYSICS

MAIN EXAMINATION 2016/2017

TITLE OF PAPER : ELECTROMAGNETIC THEORY

COURSE NUMBER : P331

TIME ALLOWED : THREE HOURS

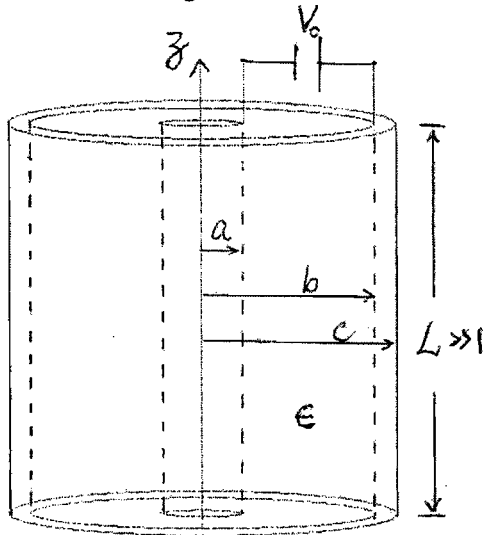
INSTRUCTIONS : ANSWER ANY FOUR OUT OF FIVE
QUESTIONS.
EACH QUESTION CARRIES 25 MARKS.

MARKS FOR DIFFERENT SECTIONS ARE
SHOWN IN THE RIGHT-HAND MARGIN.

THIS PAPER HAS TEN PAGES, INCLUDING THIS PAGE.

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GIVEN BY THE INVIGILATOR.

A very long straight coaxial cable, with an inner solid wire of radius a and an outer hollow wire with inner radius b and outer radius c , is given a potential difference V_0 across the wires. In between the wires ($a < \rho < b$) is filled with a layer of insulating material with permittivity ϵ as shown in the figure below.



- (a) From $\nabla^2 f(\rho) = 0$ with boundary conditions of $f(\rho = a) = 0$ and $f(\rho = b) = V_0$, find the specific solution of $f(\rho)$ and show that

$$f(\rho) = \frac{V_0}{\ln\left(\frac{b}{a}\right)} \ln\left(\frac{\rho}{a}\right) . \quad (9 \text{ marks})$$

- (b) Find the electric field \vec{E} from $f(\rho)$ obtained in (a). (3 marks)

- (c) (i) Find the surface conduction charge density ρ_s on $\rho = a$ and $\rho = b$ conducting surfaces respectively. Then find the total charges deposited on both surfaces, if the total cable length is L , and show that they are equal and opposite.

(4+4 marks)

(Hint : For the conducting surfaces in contact with the dielectric region of ϵ , then

$\rho_s = \vec{e}_n \cdot (\epsilon \vec{E})$ where \vec{e}_n is the normal outward unit vector on conductor surface.)

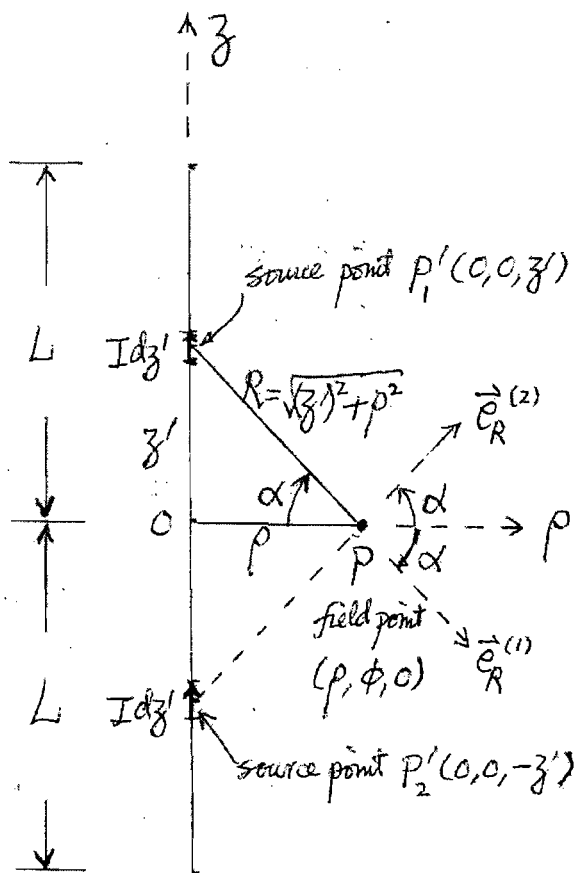
- (ii) Write down the capacitance C as well as the distributive capacitance c_d of the given coaxial cable. Show that

$$c_d = \frac{2\pi\epsilon}{\ln\left(\frac{b}{a}\right)} . \quad (2 \text{ marks})$$

- (iii) If given the values of $a = 2 \text{ mm}$, $b = 8 \text{ mm}$ & $\epsilon = 3\epsilon_0$, calculate the value of c_d .

(3 marks)

- (a) A thin conducting wire of length $2L$, with its central axis coinciding with the z -axis and its centre point coinciding with the origin, carries a steady total current I along positive z -direction as shown in the figure below.



- (i) Since the given current source is only along z -axis the vector potential at $P(\rho, \phi, 0)$ is also having only z component A_z , i.e.,

$$\vec{A} = \vec{e}_z A_z \quad \text{where} \quad A_z = \int_{z'=-L}^{z'=+L} \frac{\mu_0 I dz'}{4\pi R} = 2 \int_{z'=0}^{z'=+L} \frac{\mu_0 I dz'}{4\pi \sqrt{(z')^2 + \rho^2}}$$

carry out the above integral for A_z about z' and show that

$$A_z = \frac{\mu_0 I}{2\pi} \ln \left(\frac{L + \sqrt{L^2 + \rho^2}}{\rho} \right) \quad (8 \text{ marks})$$

(Hint: set $z' = \rho \tan(\alpha)$, $\int \sec(\alpha) d\alpha = \ln(\sec(\alpha) + \tan(\alpha))$)

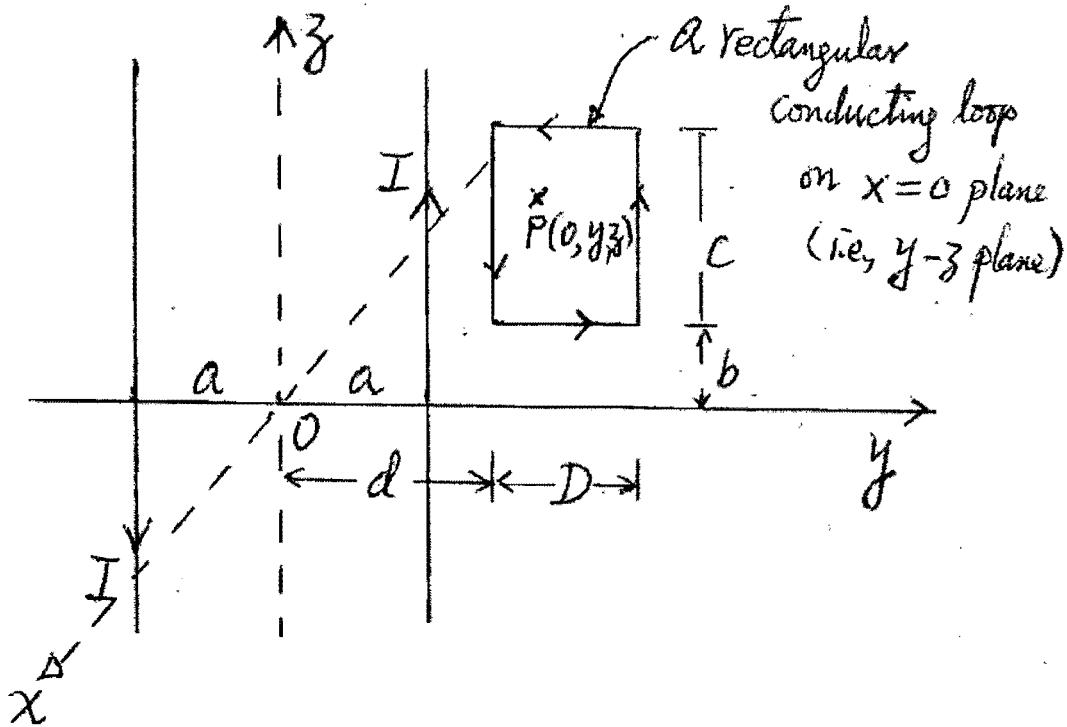
- (ii) For $L \gg \rho$ use $\vec{A} \approx \vec{e}_z \frac{\mu_0 I}{2\pi} \ln \left(\frac{2L}{\rho} \right)$ and $\vec{B} = \vec{\nabla} \times \vec{A}$ to show that

$$\vec{B} = \vec{e}_\phi \frac{\mu_0 I}{2\pi \rho} \quad (5 \text{ marks})$$

Question two (continued)

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- (b) Two very long thin conducting wires parallel to z -axis and lying on the $x = 0$ plane, i.e., $y-z$ plane, one situated at $y = -a$ and carries a current I A along $-z$ direction and the other situated at $y = +a$ and carries a current I A along $+z$ direction as shown in the following diagram.



A rectangular conducting loop of dimension $D \times c$ is placed on $x = 0$ plane and a distance of d away from the z -axis as shown in the above diagram.

- (i) Utilize the result in (a)(ii), apply the superposition principle to deduce that the magnetic field at point $P : (0, y, z)$ within the rectangular loop due to the two parallel conducting wires is

$$\vec{B}(0, y, z) = \vec{e}_x \frac{\mu_0 I}{2\pi} \left(\frac{1}{y+a} - \frac{1}{y-a} \right) \quad (4 \text{ marks})$$

(Hint: on $x = 0$ plane $\vec{e}_\phi = -\vec{e}_x$)

- (ii) Find the total magnetic flux $\Phi_m = \int_S \vec{B} \cdot d\vec{s}$ passing through the surface area confined by the rectangular loop, i.e., $S : x = 0, d \leq y \leq d + D, b \leq z \leq b + c$ and $d\vec{s} = \vec{e}_x dy dz$, in terms of μ_0, a, b, c, d, D & I . Show that the mutual inductance between the rectangular loop and the parallel wires is

$$M = \frac{\mu_0 c}{2\pi} \ln \left(\frac{(d+D+a)(d-a)}{(d+D-a)(d+a)} \right) \quad (8 \text{ marks})$$

Question three

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- (a) Apply an electric field \vec{E} to a pure conducting solid material. According to modified Drude's model, the equation of motion for an average conduction electron in the solid material can be written as

$$m_e \frac{d\vec{v}_d}{dt} = -e \vec{E} - \frac{2 m_e \vec{v}_d}{\tau_f}$$

where $-e$ & m_e are the electron charge and mass respectively.

- (i) Explain briefly the meanings of \vec{v}_d , τ_f and $-\frac{2 m_e \vec{v}_d}{\tau_f}$. (3 marks)

- (ii) In the steady state case, i.e., $\frac{d\vec{v}_d}{dt} = 0$, deduce the following point form of

Ohm's law $\vec{J} = \sigma \vec{E}$ where $\sigma = \frac{n e^2}{2 m_e} \tau_f$ and n is the number density of the

conduction electrons in the material. (6 marks)

(Hint : $\vec{J} = \rho_v \vec{v}_d = -n e \vec{v}_d$)

- (iii) Pure solid Ruthenium Ru has an atomic weight = 101.07 kg / kg-mole, a density = 12200 kg/m³ and a conductivity $\sigma = 1.4 \times 10^7 \Omega^{-1} m^{-1}$ at room temperature.

- (A) Find the number of conduction electrons per meter cube, i.e., number density n , for metal Ru if each Ru atom contributes two conduction electrons. (4 marks)

(Hint : one kg-mole pure metal contains 6.022×10^{26} atoms)

- (B) Find the value of τ_f for Ru metal at room temperature. (4 marks)

- (b) The Maxwell's equations for a material region with parameters of (μ, ϵ, σ) are

$$\left\{ \begin{array}{l} \vec{\nabla} \cdot \vec{E}(space, t) = 0 \quad \dots\dots (1) \\ \vec{\nabla} \cdot \vec{H}(space, t) = 0 \quad \dots\dots (2) \\ \vec{\nabla} \times \vec{E}(space, t) = -\mu \frac{\partial \vec{H}(space, t)}{\partial t} \quad \dots\dots (3) \\ \vec{\nabla} \times \vec{H}(space, t) = \sigma \vec{E}(space, t) + \epsilon \frac{\partial \vec{E}(space, t)}{\partial t} \quad \dots\dots (4) \end{array} \right.$$

- (i) Setting $\vec{E}(space, t) = \vec{\tilde{E}}(space) e^{i\omega t}$ & $\vec{H}(space, t) = \vec{\tilde{H}}(space) e^{i\omega t}$, deduce the following time-harmonic Maxwell's equations :

$$\left\{ \begin{array}{l} \vec{\nabla} \cdot \vec{\tilde{E}}(space) = 0 \quad \dots\dots (5) \\ \vec{\nabla} \cdot \vec{\tilde{H}}(space) = 0 \quad \dots\dots (6) \\ \vec{\nabla} \times \vec{\tilde{E}}(space) = -i\omega\mu \vec{\tilde{H}}(space) \quad \dots\dots (7) \\ \vec{\nabla} \times \vec{\tilde{H}}(space) = (\sigma + i\omega\epsilon) \vec{\tilde{E}}(space) \quad \dots\dots (8) \end{array} \right.$$

(3 marks)

- (ii) From equations in (b)(i) deduce the following wave equation for $\vec{\tilde{H}}(space)$ as

$$\nabla^2 \vec{\tilde{H}}(space) = \hat{\gamma}^2 \vec{\tilde{H}}(space) \text{ where } \hat{\gamma} = \sqrt{i\omega\mu(\sigma + i\omega\epsilon)} \quad (5 \text{ marks})$$

Question four

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- (a) A uniform plane wave traveling along +z direction with the field components $E_x(z)$ & $H_y(z)$ has a complex electric field amplitude $\hat{E}_m^+ = 80 e^{i40^\circ}$ V/m and propagates at a frequency $f = 6 \times 10^5$ Hz in a material region has the parameters of $\mu = \mu_0$, $\epsilon = 4 \epsilon_0$ & $\frac{\sigma}{\omega \epsilon} = 0.7$.

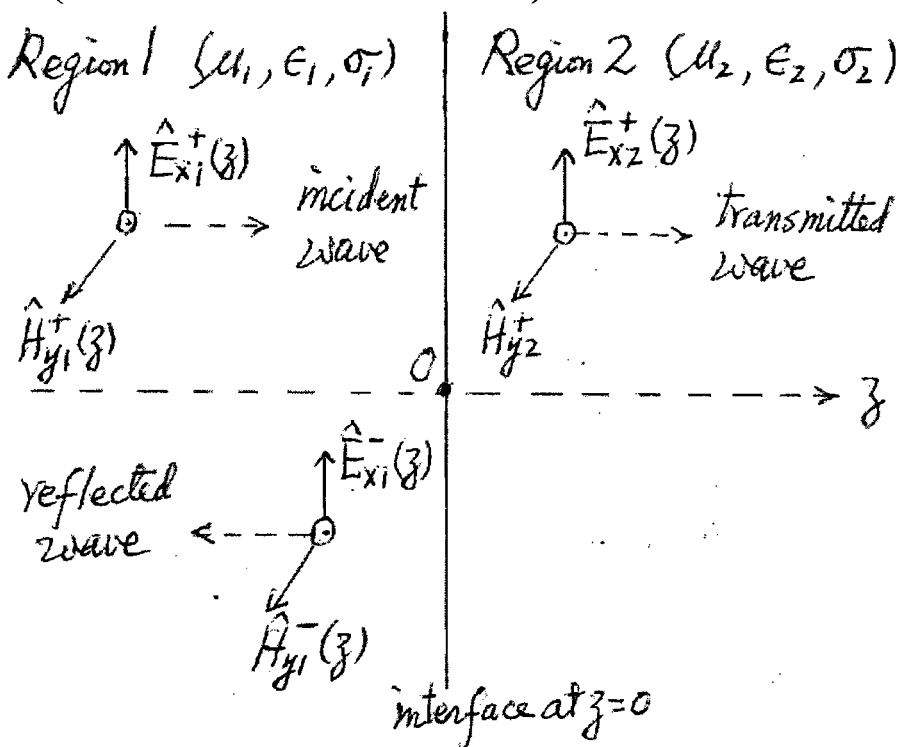
- (i) Find the values of the propagation constant $\hat{\gamma} (= \alpha + i \beta)$ and the intrinsic wave impedance $\hat{\eta}$ for this wave. **(4 marks)**
- (ii) Express the electric and magnetic fields in both their complex and real-time forms, with the numerical values of (a)(i) inserted. **(4 marks)**
- (iii) Find the values of the penetration depth, wave length and phase velocity of the given wave. **(3 marks)**

- (b) An uniform plane wave is incident normally upon an interface separating two regions.

The incident wave is given as $\left(\hat{E}_{x1}^+ = \hat{E}_{m1}^+ e^{-\hat{\gamma}_1 z}, \hat{H}_{y1}^+ = \frac{\hat{E}_{m1}^+}{\hat{\eta}_1} e^{-\hat{\gamma}_1 z} \right)$ and thus the

reflected and transmitted wave can be written as $\left(\hat{E}_{x1}^- = \hat{E}_{m1}^- e^{+\hat{\gamma}_1 z}, \hat{H}_{y1}^- = -\frac{\hat{E}_{m1}^-}{\hat{\eta}_1} e^{+\hat{\gamma}_1 z} \right)$

and $\left(\hat{E}_{x2}^+ = \hat{E}_{m2}^+ e^{-\hat{\gamma}_2 z}, \hat{H}_{y2}^+ = \frac{\hat{E}_{m2}^+}{\hat{\eta}_2} e^{-\hat{\gamma}_2 z} \right)$ respectively as shown below:



Question four (continued)

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- (i) From the boundary conditions at the interface , i.e., both total \hat{E}_x & \hat{H}_y are continuous at $z = 0$, deduce the following

$$\begin{cases} \hat{E}_{m1}^- = \hat{E}_{m1}^+ \frac{\hat{\eta}_2 - \hat{\eta}_1}{\hat{\eta}_2 + \hat{\eta}_1} \\ \hat{E}_{m2}^+ = \hat{E}_{m1}^+ \frac{2\hat{\eta}_2}{\hat{\eta}_2 + \hat{\eta}_1} \end{cases} \quad (8 \text{ marks})$$

- (ii) If region 1 is air (i.e., $\hat{\eta}_1 = 120 \pi = 377 \Omega$), region 2 is a lossy medium with parameters of $\left(\mu_2 = \mu_0, \epsilon_2 = 9 \epsilon_0, \frac{\sigma_2}{\omega \epsilon_2} = 1 \right)$, and the incident plane wave is having a complex amplitude of $\hat{E}_{m1}^+ = 100 e^{i50^\circ}$ V/m and propagates at a frequency of $f = 10^6$ Hz .

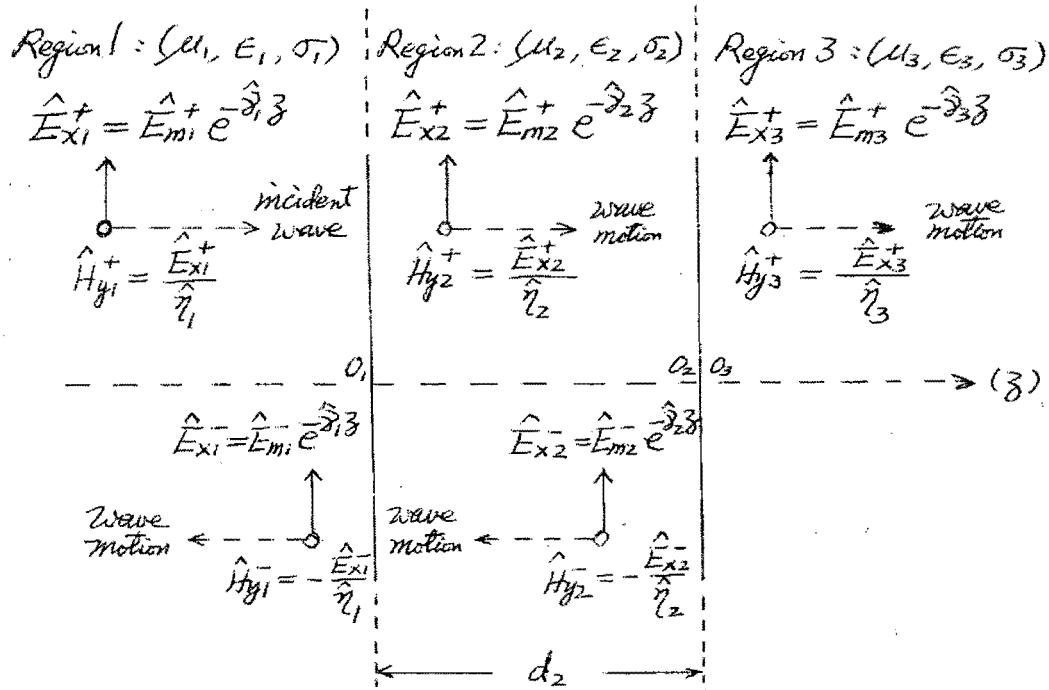
(A) Calculate the value of $\hat{\eta}_2$. (2 marks)

(B) Calculate the values of \hat{E}_{m1}^- . (4 marks)

Question five

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A uniform plane wave $(\hat{E}_{x1}^+, \hat{H}_{y1}^+)$, with a frequency f , is incident normally on a layer of thickness d_2 , and emerges into region 3 as shown below :



0_1 , 0_2 & 0_3 are the respective origins for region 1, 2 & 3 chosen at the first and second interface.

- (a) Define for the i^{th} region ($i=1,2,3$) the reflection coefficient $\hat{\Gamma}_i(z)$ and the total wave impedance $\hat{Z}_i(z)$ and deduce the following :

$$\begin{cases} \hat{Z}_i(z) = \hat{\eta}_i \frac{1 + \hat{\Gamma}_i(z)}{1 - \hat{\Gamma}_i(z)} \\ \hat{\Gamma}_i(z') = \hat{\Gamma}_i(z) e^{2\hat{\gamma}_i(z'-z)} \end{cases} \quad \text{where } z' \text{ \& } z \text{ are two positions in } i^{th} \text{ region} \quad (2 + 7 \text{ marks})$$

- (b) If $f = 10^7$ Hz and $d_2 = \frac{\lambda_2}{4}$, region 1 & 3 are air regions and region 2 is a lossless

region with parameters $\mu_2 = \mu_0$, $\epsilon_1 = 16 \epsilon_0$ & $\frac{\sigma}{\omega \epsilon} = 0$,

- (i) find the values of β_1 , β_2 , β_3 , λ_2 & $\hat{\eta}_2$, (note : $\hat{\eta}_1 = \hat{\eta}_3 = 120 \pi \Omega$ and $\alpha_1 = \alpha_2 = \alpha_3 = 0$) (4 marks)

- (ii) starting with $\hat{\Gamma}_3(z) = 0$ for the rightmost region, i.e., region 3, and using continuous \hat{Z} at the interface as well as the equations in (a), find the values of $\hat{Z}_3(0)$, $\hat{Z}_2(0)$, $\hat{\Gamma}_2(0)$, $\hat{\Gamma}_2(-d_2)$, $\hat{Z}_2(-d_2)$, $\hat{Z}_1(0)$ & $\hat{\Gamma}_1(0)$

(10 marks)

- (iii) find the value of \hat{E}_{m1}^- if given $\hat{E}_{m1}^+ = 50$ V/m.

(2 marks)

Useful informations

$$e = 1.6 \times 10^{-19} \text{ C}$$

$$m_e = 9.1 \times 10^{-31} \text{ kg}$$

$$\mu_0 = 4 \pi \times 10^{-7} \frac{\text{H}}{\text{m}}$$

$$\varepsilon_0 = 8.85 \times 10^{-12} \frac{\text{F}}{\text{m}}$$

$$\alpha = \frac{\omega \sqrt{\mu \varepsilon}}{\sqrt{2}} \sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} - 1$$

$$\beta = \frac{\omega \sqrt{\mu \varepsilon}}{\sqrt{2}} \sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} + 1$$

$$\frac{1}{\sqrt{\mu_0 \varepsilon_0}} = 3 \times 10^8 \frac{\text{m}}{\text{s}}$$

$$\hat{\eta} = \frac{\sqrt{\frac{\mu}{\varepsilon}}}{\sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2}} e^{i \frac{1}{2} \tan^{-1} \left(\frac{\sigma}{\omega \varepsilon}\right)}$$

$$\eta_0 = \sqrt{\frac{\mu_0}{\varepsilon_0}} = 120 \pi \ \Omega = 377 \ \Omega$$

$$\beta_0 = \omega \sqrt{\mu_0 \varepsilon_0}$$

$$\oiint_S \vec{E} \cdot d\vec{s} = \frac{1}{\varepsilon} \iiint_V \rho_v \, dv$$

$$\oiint_S \vec{B} \cdot d\vec{s} \equiv 0$$

$$\oint_L \vec{E} \cdot d\vec{l} = - \frac{\partial}{\partial t} \left(\iint_S \vec{B} \cdot d\vec{s} \right)$$

$$\oint_L \vec{B} \cdot d\vec{l} = \mu \iint_S \vec{J} \cdot d\vec{s} + \mu \varepsilon \frac{\partial}{\partial t} \left(\iint_S \vec{E} \cdot d\vec{s} \right)$$

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho_v}{\varepsilon}$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{E} = - \frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{B} = \mu \vec{J} + \mu \varepsilon \frac{\partial \vec{E}}{\partial t}$$

$$\vec{J} = \sigma \vec{E}$$

$$\vec{D} = \varepsilon \vec{E} = \varepsilon_0 \vec{E} + \vec{P} \quad \& \quad \vec{B} = \mu \vec{H} = \mu_0 \vec{H} + \vec{M} \quad 112.$$

$$\oiint_S \vec{F} \cdot d\vec{s} \equiv \iiint_V (\vec{\nabla} \cdot \vec{F}) dV \quad \text{divergence theorem}$$

$$\oint_L \vec{F} \cdot d\vec{l} \equiv \iint_S (\vec{\nabla} \times \vec{F}) \cdot d\vec{s} \quad \text{Stokes' theorem}$$

$$\vec{\nabla} \cdot (\vec{\nabla} \times \vec{F}) \equiv 0$$

$$\vec{\nabla} \times (\vec{\nabla} f) \equiv 0$$

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{F}) \equiv \vec{\nabla} (\vec{\nabla} \cdot \vec{F}) - \nabla^2 \vec{F}$$

$$\vec{\nabla} f = \vec{e}_x \frac{\partial f}{\partial x} + \vec{e}_y \frac{\partial f}{\partial y} + \vec{e}_z \frac{\partial f}{\partial z} = \vec{e}_\rho \frac{\partial f}{\partial \rho} + \vec{e}_\phi \frac{1}{\rho} \frac{\partial f}{\partial \phi} + \vec{e}_z \frac{\partial f}{\partial z}$$

$$= \vec{e}_r \frac{\partial f}{\partial r} + \vec{e}_\theta \frac{1}{r} \frac{\partial f}{\partial \theta} + \vec{e}_\phi \frac{1}{r \sin(\theta)} \frac{\partial f}{\partial \phi}$$

$$\vec{\nabla} \cdot \vec{F} = \frac{\partial(F_x)}{\partial x} + \frac{\partial(F_y)}{\partial y} + \frac{\partial(F_z)}{\partial z} = \frac{1}{\rho} \frac{\partial(F_\rho \rho)}{\partial \rho} + \frac{1}{\rho} \frac{\partial(F_\phi)}{\partial \phi} + \frac{\partial(F_z)}{\partial z}$$

$$= \frac{1}{r^2} \frac{\partial(F_r r^2)}{\partial r} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\theta \sin(\theta))}{\partial \theta} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\phi)}{\partial \phi}$$

$$\vec{\nabla} \times \vec{F} = \vec{e}_x \left(\frac{\partial(F_z)}{\partial y} - \frac{\partial(F_y)}{\partial z} \right) + \vec{e}_y \left(\frac{\partial(F_x)}{\partial z} - \frac{\partial(F_z)}{\partial x} \right) + \vec{e}_z \left(\frac{\partial(F_y)}{\partial x} - \frac{\partial(F_x)}{\partial y} \right)$$

$$= \frac{\vec{e}_\rho}{\rho} \left(\frac{\partial(F_z)}{\partial \phi} - \frac{\partial(F_\phi \rho)}{\partial z} \right) + \vec{e}_\phi \left(\frac{\partial(F_\rho)}{\partial z} - \frac{\partial(F_z)}{\partial \rho} \right) + \frac{\vec{e}_z}{\rho} \left(\frac{\partial(F_\phi \rho)}{\partial \rho} - \frac{\partial(F_\rho)}{\partial \phi} \right)$$

$$= \frac{\vec{e}_r}{r^2 \sin(\theta)} \left(\frac{\partial(F_\phi r \sin(\theta))}{\partial \theta} - \frac{\partial(F_\theta r)}{\partial \phi} \right) + \frac{\vec{e}_\theta}{r \sin(\theta)} \left(\frac{\partial(F_r)}{\partial \phi} - \frac{\partial(F_\phi r \sin(\theta))}{\partial r} \right) + \frac{\vec{e}_\phi}{r} \left(\frac{\partial(F_\theta r)}{\partial r} - \frac{\partial(F_r)}{\partial \theta} \right)$$

where $\vec{F} = \vec{e}_x F_x + \vec{e}_y F_y + \vec{e}_z F_z = \vec{e}_\rho F_\rho + \vec{e}_\phi F_\phi + \vec{e}_z F_z = \vec{e}_r F_r + \vec{e}_\theta F_\theta + \vec{e}_\phi F_\phi$ and

$$d\vec{l} = \vec{e}_x dx + \vec{e}_y dy + \vec{e}_z dz = \vec{e}_\rho d\rho + \vec{e}_\phi \rho d\phi + \vec{e}_z dz = \vec{e}_r dr + \vec{e}_\theta r d\theta + \vec{e}_\phi r \sin(\theta) d\phi$$

$$\nabla^2 f = \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2} = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\rho \frac{\partial f}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 f}{\partial \phi^2} + \frac{\partial^2 f}{\partial z^2}$$

$$= \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial f}{\partial r} \right) + \frac{1}{r^2 \sin(\theta)} \frac{\partial}{\partial \theta} \left(\sin(\theta) \frac{\partial f}{\partial \theta} \right) + \frac{1}{r^2 \sin^2(\theta)} \frac{\partial^2 f}{\partial \phi^2}$$

$$\hat{Z}_i(z) = \hat{\eta}_i \frac{1 + \hat{\Gamma}_i(z)}{1 - \hat{\Gamma}_i(z)} \quad , \quad \hat{\Gamma}_i(z) = \frac{\hat{Z}_i(z) - \hat{\eta}_i}{\hat{Z}_i(z) + \hat{\eta}_i} \quad \&$$

$$\hat{\Gamma}_i(z') = \hat{\Gamma}_i(z) e^{2\hat{\eta}_i(z'-z)} \quad \text{where } z' \text{ \& } z \text{ are two positions in } i^{\text{th}} \text{ region}$$