

UNIVERSITY OF SWAZILAND

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FACULTY OF SCIENCE AND ENGINEERING

DEPARTMENT OF PHYSICS

SUPPLEMENTARY EXAMINATION 2016/2017

TITLE OF PAPER : ELECTROMAGNETIC THEORY

COURSE NUMBER : P331

TIME ALLOWED : THREE HOURS

INSTRUCTIONS : ANSWER ANY FOUR OUT OF FIVE
QUESTIONS.
EACH QUESTION CARRIES 25 MARKS.

MARKS FOR DIFFERENT SECTIONS ARE
SHOWN IN THE RIGHT-HAND MARGIN.

THIS PAPER HAS ELEVEN PAGES, INCLUDING THIS PAGE.

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GIVEN BY THE INVIGILATOR.

Question one

(a) A dielectric spherical ball of radius R_0 with a permittivity ϵ , centered at the origin and embedded in air of permittivity ϵ_0 , carries a volume charge density distribution of $\rho_v = 10(1 + \alpha r^2) \text{ C/m}^3$ where α is a constant.

(i) Find the total electric charge Q_0 of the dielectric spherical ball in terms of R_0 & α and show that

$$Q_0 = 4\pi \left(\frac{10}{3} R_0^3 + 2\alpha R_0^5 \right) \quad \text{(3 marks)}$$

(Hint: $dv = r^2 \sin(\theta) dr d\theta d\phi$)

(ii) Set $\vec{E} = \vec{e}_r E_r(r)$ (make a brief justification of this setting), use the integral form of Gauss's law and choose and draw proper Gaussian surfaces to find \vec{E} in terms of r , R_0 & α for $0 \leq r \leq R_0$ & $r \geq R_0$ regions. **(1+1+6 marks)**

(iii) Find the value of α in terms of R_0 such that the electric field everywhere outside the spherical ball is zero. **(2 marks)**

(b) A positron of charge $+e$ having an initial constant velocity $\vec{e}_x v_0$ and projected into a constant electric and magnetic field $\vec{E} = \vec{e}_x E_0$ and $\vec{B} = \vec{e}_y B_0$, taking its entrance position as the origin of Cartesian coordinate and entrance moment as $t = 0$, its

equation of motion is $m_e \frac{d\vec{v}(t)}{dt} = e\vec{E} + e\vec{v}(t) \times \vec{B}$ (1) where

$$\vec{v}(t) = \vec{e}_x v_x(t) + \vec{e}_y v_y(t) + \vec{e}_z v_z(t)$$

(i) Decompose eq.(1) into three scalar differential equations and deduce that

$$\left\{ \begin{array}{l} m_e \frac{dv_x(t)}{dt} = eE_0 - e v_z(t) B_0 \quad \text{..... (2)} \\ m_e \frac{dv_y(t)}{dt} = 0 \quad \text{..... (3)} \\ m_e \frac{dv_z(t)}{dt} = e v_x(t) B_0 \quad \text{..... (4)} \end{array} \right.$$

(3 marks)

(ii) Eq.(2) & eq.(4) are coupled differential equations for $v_x(t)$ & $v_z(t)$. De-couple them and deduce that

$$\frac{d^2 v_x(t)}{dt^2} = -\omega^2 v_x(t) \quad \text{where} \quad \omega = \frac{e B_0}{m_e} \quad \text{..... (5)} \quad \text{(3 marks)}$$

Question one (continued)

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(iii) The general solution of $v_x(t)$ from eq.(5) can be written as

$$v_x(t) = k_1 \cos(\omega t) + k_2 \sin(\omega t) \dots\dots (6)$$

where k_1 & k_2 are arbitrary constants.

Substitute eq.(6) into eq.(2) and deduce that the general solution of $v_z(t)$ is

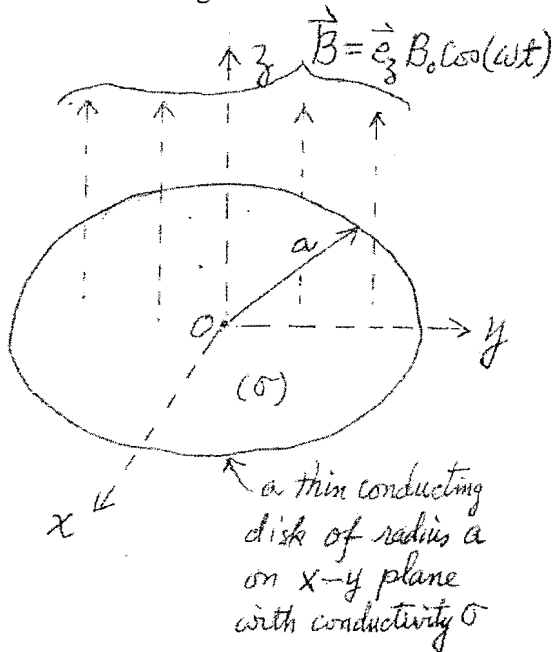
$$v_z(t) = \frac{E_0}{B_0} + k_1 \sin(\omega t) - k_2 \cos(\omega t) \dots\dots (7) \quad (2 \text{ marks})$$

(iv) From the given initial conditions of $v_x(t)$ & $v_z(t)$, i.e., $v_x(0) = v_0$ & $v_z(0) = 0$, and the general solutions of $v_x(t)$ & $v_z(t)$, i.e., eq.(6) & eq.(7), find the values of k_1 & k_2 in terms of v_0 , E_0 & B_0 and then write down the specific solutions of $v_x(t)$ & $v_z(t)$. (3+1 marks)

Question two

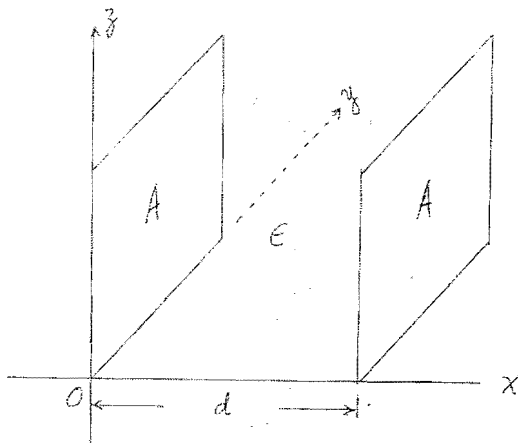
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- (a) A very thin conducting disk of radius a and conductivity σ is placed on x - y plane and centred at the origin as shown in the following diagram



A time-dependent magnetic field $\vec{B} = \vec{a}_z B_0 \cos(\omega t)$, where B_0 & ω are constants, is applied to the conducting disk.

- (i) Set the induced electric field in the conducting disk as $\vec{E} = \vec{e}_\phi E_\phi(\rho)$ (provide a brief justification), use the integral form of Faraday's law, and draw appropriate closed loop to deduce that $\vec{E} = \vec{e}_\phi E_\phi(\rho)$. (1+1+8 marks)
- (ii) Based on the result of (a)(i), write down the induced current density in the conducting disk. (1 mark)
- (b) A two-parallel conducting plate capacitor system is shown in the following diagram



where A is the plate surface area, d is the plate separation and ϵ is the dielectric constant of the insulating material layer in-between the two plates.

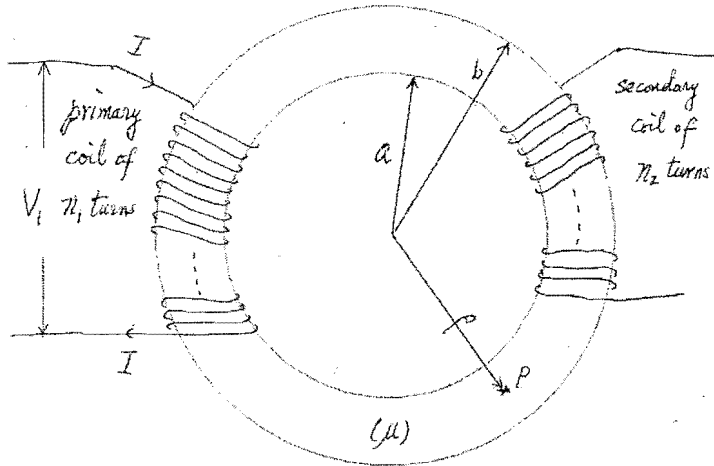
Question two (continued)

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- (i) From $\nabla^2 f(x) = 0$ with boundary conditions of $f(x=0) = 0$ and $f(x=d) = V_0$, find the specific solution of $f(x)$. (4 marks)
- (ii) Find \vec{E} from $f(x)$ obtained in (b)(i) and then write down \vec{D} & \vec{P} in-between the two conducting plates. (4 marks)
- (iii) Use $\rho_s = D_n$ where ρ_s & D_n are the surface conduction charge density and normal outward \vec{D} component on the conductor's surface respectively, find ρ_s on both $x=0$ and $x=d$ conductor's surfaces respectively. Then find the total charge on both surfaces with surface area A and show that they are equal and opposite. (5 marks)
- (iv) Write down the capacitance of this two-parallel conducting plate capacitor system. (1 mark)

Question three

A static current I flows in the primary coil of n_1 turn toroid, wired around an iron ring core of magnetic permeability μ with the square cross-section area $(b - a)^2$ as shown below:



where z -axis is pointing out of this paper.

- (a) Set $\vec{B} = \vec{e}_\phi B_\phi(\rho)$ (justify this briefly) and use the integral form of Ampere's law (choose and draw proper closed loops) to find the magnetic field \vec{B} within the iron core, i.e., $a \leq \rho \leq b$ & $0 \leq z \leq (b - a)$ region. Show that

$$\vec{B} = -\vec{a}_\phi \frac{\mu n_1 I}{2\pi \rho} \quad \text{within the iron core.} \quad (1+1+5 \text{ marks})$$

- (b) Find the total magnetic flux Ψ_m passing through the cross-section area $(b - a)^2$ of the iron ring in counter clockwise sense, i.e., $\int_S \vec{B} \cdot d\vec{s}$ where $S: a \leq \rho \leq b$, $0 \leq z \leq (b - a)$ & $d\vec{s} = \vec{a}_\phi d\rho dz$, in terms of a, b, n_1, μ & I , i.e.,

$$\text{show that } \Psi_m = -\frac{\mu n_1 I}{2\pi} \times \ln\left(\frac{b}{a}\right) \times (b - a) \quad (4 \text{ marks})$$

- (c) Find the self-inductance L of the primary coil as well as the mutual inductance M of the secondary coil due to the primary coil in terms of a, b, μ, n_1 & n_2 .

(5 marks)

- (d) (i) If the primary coil carries a sinusoidal current of $I_0 \sin(\omega t)$ instead of carrying a static current I , find the induced e.m.f. $V_2(t)$ in the secondary coil in terms of $a, b, \omega, n_1, n_2, \mu$ & I_0 under quasi static situation. (5 marks)

- (ii) If the potential drop for the primary coil due to its resistance is negligible compared to the one due to its self-inductance, i.e., $V_1(t) \approx L \frac{dI}{dt}$, show that

$$\frac{|V_2(t)|}{|V_1(t)|} = \frac{n_2}{n_1} \quad (4 \text{ marks})$$

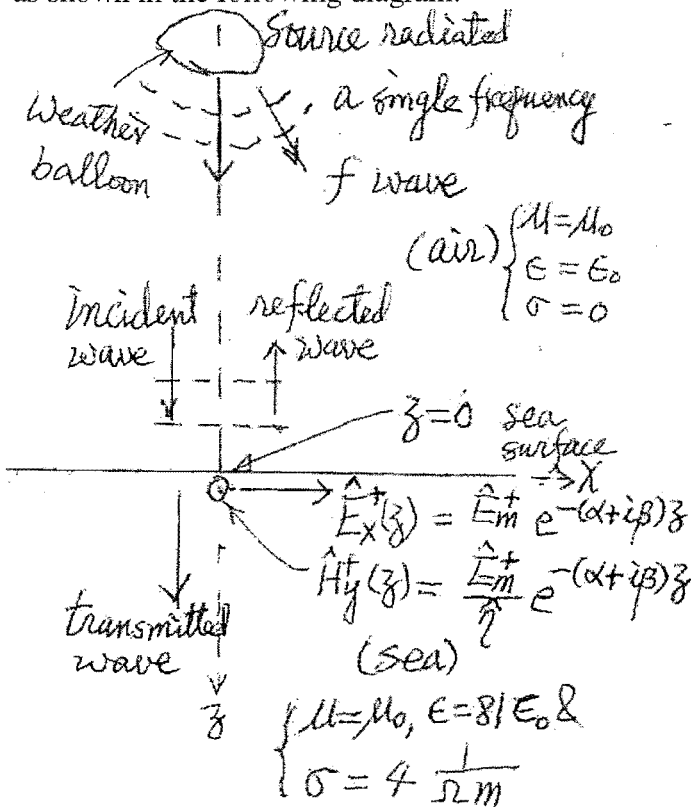
Question four

- (a) (i) For any closed surface S , enclosing a volume V , the integral form of the continuity equation for electric charges in Electromagnetic theory can be written as $\oint_S \vec{J} \cdot d\vec{s} = -\frac{d}{dt} \left(\oint_V \rho_v dv \right)$. Explain briefly the meaning of the left hand side and the right hand side of this equation and indicate which law in physics it describes. **(3+1 marks)**
- (ii) Use the divergence theorem to transform the above integral form of continuity equation for electric charges into its differential form. **(3 marks)**
- (iii) (A) Show that without introducing the displacement current term, i.e., $\frac{\partial \vec{D}}{\partial t}$, in the equation for Ampere's law, i.e., $\vec{\nabla} \times \vec{H} = \vec{J}$ instead of $\vec{\nabla} \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$, Maxwell's equations would contradict the continuity equation for electric charges. **(2 marks)**
- (B) Show that by including the displacement current term, Maxwell's equations are in agreement with the continuity equation. **(4 marks)**
- (b) (i) From the time-dependent Maxwell's equations deduce the following wave equation for \vec{E} in the material region with parameters of μ , ϵ & σ where $\rho_v = 0$ & $\vec{J} = \sigma \vec{E}$, as
- $$\nabla^2 \vec{E} = \mu \sigma \frac{\partial \vec{E}}{\partial t} + \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2} \quad \text{(6 marks)}$$
- (ii) By direct substitution, show that $E_x = \hat{E}_m e^{\hat{\gamma}z} e^{i\omega t}$ (where \hat{E}_m is any constant, ω is any frequency and $\hat{\gamma} = \sqrt{i\omega\mu\sigma - \omega^2\mu\epsilon}$) is a solution to the E_x part of the wave equation in (a)(i), i.e., $\nabla^2 E_x = \mu \sigma \frac{\partial E_x}{\partial t} + \mu \epsilon \frac{\partial^2 E_x}{\partial t^2}$. **(6 marks)**

Question five

12.7

A stationary weather balloon, high above the sea surface (taken as $z = 0$ plane), radiates a spherical wave of frequency f . When the radiated wave reaches the sea surface directly below the balloon, it can be considered as a uniform plane wave incident normally upon the sea surface, locally at least, as shown in the following diagram.



Assuming the sea water has the constants $\mu = \mu_0$, $\epsilon = 81\epsilon_0$ & $\sigma = 4 \Omega^{-1} m^{-1}$ and

$$\hat{E}_x^+(0) = \hat{E}_m^+ = 1 \text{ V/m.}$$

(a) If $f = 10^4$ Hz (i.e., in the very low frequency VLF range),

- (i) find the values of the loss tangent $\frac{\sigma}{\omega \epsilon}$, the propagation constant $\hat{\gamma} (= \alpha + i\beta)$ and the intrinsic wave impedance $\hat{\eta}$ for this wave at this frequency in the sea, (2+2+2 marks)
- (ii) express the electric and magnetic fields in both their complex and real-time forms, with the numerical values of (a)(i) inserted for this transmitted wave, and (6 marks)
- (iii) find the values of the penetration depth, the wave length and phase velocity of the given wave at this frequency in the sea. (3 marks)

Question five (continued)

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- (b) If $f = 1000$ Hz (i.e., in the extremely low frequency ELF range),
- (i) find the values of the loss tangent $\frac{\sigma}{\omega \epsilon}$, the propagation constant $\hat{\gamma} (= \alpha + i \beta)$ and the intrinsic wave impedance $\hat{\eta}$ for this wave at this frequency in the sea, and
(2+2+2 marks)
- (ii) find the values of the penetration depth, the wave length and phase velocity of the given wave at this frequency in the sea.
(3 marks)
- (c) Based on the results of (a)(iii) and (b)(ii), comment on the effectiveness of undersea radio communication.
(1 mark)

Useful informations

$$e = 1.6 \times 10^{-19} \text{ C}$$

$$m_e = 9.1 \times 10^{-31} \text{ kg}$$

$$\mu_0 = 4 \pi \times 10^{-7} \frac{\text{H}}{\text{m}}$$

$$\varepsilon_0 = 8.85 \times 10^{-12} \frac{\text{F}}{\text{m}}$$

$$\alpha = \frac{\omega \sqrt{\mu \varepsilon}}{\sqrt{2}} \sqrt{\sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} - 1}$$

$$\beta = \frac{\omega \sqrt{\mu \varepsilon}}{\sqrt{2}} \sqrt{\sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} + 1}$$

$$\frac{1}{\sqrt{\mu_0 \varepsilon_0}} = 3 \times 10^8 \frac{\text{m}}{\text{s}}$$

$$\hat{\eta} = \frac{\sqrt{\frac{\mu}{\varepsilon}}}{\sqrt[4]{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2}} e^{i \frac{1}{2} \tan^{-1}\left(\frac{\sigma}{\omega \varepsilon}\right)}$$

$$\eta_0 = \sqrt{\frac{\mu_0}{\varepsilon_0}} = 120 \pi \quad \Omega = 377 \quad \Omega$$

$$\beta_0 = \omega \sqrt{\mu_0 \varepsilon_0}$$

$$\oiint_S \vec{E} \cdot d\vec{s} = \frac{1}{\varepsilon} \iiint_V \rho_v \, dv$$

$$\oiint_S \vec{B} \cdot d\vec{s} = 0$$

$$\oint_L \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \left(\iint_S \vec{B} \cdot d\vec{s} \right)$$

$$\oint_L \vec{B} \cdot d\vec{l} = \mu \iint_S \vec{J} \cdot d\vec{s} + \mu \varepsilon \frac{\partial}{\partial t} \left(\iint_S \vec{E} \cdot d\vec{s} \right)$$

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho_v}{\varepsilon}$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{B} = \mu \vec{J} + \mu \varepsilon \frac{\partial \vec{E}}{\partial t}$$

$$\vec{J} = \sigma \vec{E}$$

$$\vec{D} = \epsilon \vec{E} = \epsilon_0 \vec{E} + \vec{P} \quad \& \quad \vec{B} = \mu \vec{H} = \mu_0 \vec{H} + \vec{M}$$

$$\oiint_S \vec{F} \cdot d\vec{s} \equiv \iiint_V (\vec{\nabla} \cdot \vec{F}) dV \quad \text{divergence theorem}$$

$$\oint_L \vec{F} \cdot d\vec{l} \equiv \iint_S (\vec{\nabla} \times \vec{F}) \cdot d\vec{s} \quad \text{Stokes' theorem}$$

$$\vec{\nabla} \cdot (\vec{\nabla} \times \vec{F}) \equiv 0$$

$$\vec{\nabla} \times (\vec{\nabla} f) \equiv 0$$

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{F}) \equiv \vec{\nabla} (\vec{\nabla} \cdot \vec{F}) - \nabla^2 \vec{F}$$

$$\vec{\nabla} f = \vec{e}_x \frac{\partial f}{\partial x} + \vec{e}_y \frac{\partial f}{\partial y} + \vec{e}_z \frac{\partial f}{\partial z} = \vec{e}_\rho \frac{\partial f}{\partial \rho} + \vec{e}_\phi \frac{1}{\rho} \frac{\partial f}{\partial \phi} + \vec{e}_z \frac{\partial f}{\partial z}$$

$$= \vec{e}_r \frac{\partial f}{\partial r} + \vec{e}_\theta \frac{1}{r} \frac{\partial f}{\partial \theta} + \vec{e}_\phi \frac{1}{r \sin(\theta)} \frac{\partial f}{\partial \phi}$$

$$\vec{\nabla} \cdot \vec{F} = \frac{\partial(F_x)}{\partial x} + \frac{\partial(F_y)}{\partial y} + \frac{\partial(F_z)}{\partial z} = \frac{1}{\rho} \frac{\partial(F_\rho \rho)}{\partial \rho} + \frac{1}{\rho} \frac{\partial(F_\phi)}{\partial \phi} + \frac{\partial(F_z)}{\partial z}$$

$$= \frac{1}{r^2} \frac{\partial(F_r r^2)}{\partial r} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\theta \sin(\theta))}{\partial \theta} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\phi)}{\partial \phi}$$

$$\vec{\nabla} \times \vec{F} = \vec{e}_x \left(\frac{\partial(F_z)}{\partial y} - \frac{\partial(F_y)}{\partial z} \right) + \vec{e}_y \left(\frac{\partial(F_x)}{\partial z} - \frac{\partial(F_z)}{\partial x} \right) + \vec{e}_z \left(\frac{\partial(F_y)}{\partial x} - \frac{\partial(F_x)}{\partial y} \right)$$

$$= \frac{\vec{e}_\rho}{\rho} \left(\frac{\partial(F_z)}{\partial \phi} - \frac{\partial(F_\phi \rho)}{\partial z} \right) + \vec{e}_\phi \left(\frac{\partial(F_\rho)}{\partial z} - \frac{\partial(F_z)}{\partial \rho} \right) + \frac{\vec{e}_z}{\rho} \left(\frac{\partial(F_\phi \rho)}{\partial \rho} - \frac{\partial(F_\rho)}{\partial \phi} \right)$$

$$= \frac{\vec{e}_r}{r^2 \sin(\theta)} \left(\frac{\partial(F_\phi r \sin(\theta))}{\partial \theta} - \frac{\partial(F_\theta r)}{\partial \phi} \right) + \frac{\vec{e}_\theta}{r \sin(\theta)} \left(\frac{\partial(F_r)}{\partial \phi} - \frac{\partial(F_\phi r \sin(\theta))}{\partial r} \right) + \frac{\vec{e}_\phi}{r} \left(\frac{\partial(F_\theta r)}{\partial r} - \frac{\partial(F_r)}{\partial \theta} \right)$$

where $\vec{F} = \vec{e}_x F_x + \vec{e}_y F_y + \vec{e}_z F_z = \vec{e}_\rho F_\rho + \vec{e}_\phi F_\phi + \vec{e}_z F_z = \vec{e}_r F_r + \vec{e}_\theta F_\theta + \vec{e}_\phi F_\phi$ and

$$d\vec{l} = \vec{e}_x dx + \vec{e}_y dy + \vec{e}_z dz = \vec{e}_\rho d\rho + \vec{e}_\phi \rho d\phi + \vec{e}_z dz = \vec{e}_r dr + \vec{e}_\theta r d\theta + \vec{e}_\phi r \sin(\theta) d\phi$$

$$\nabla^2 f = \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2} = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\rho \frac{\partial f}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 f}{\partial \phi^2} + \frac{\partial^2 f}{\partial z^2}$$

$$= \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial f}{\partial r} \right) + \frac{1}{r^2 \sin(\theta)} \frac{\partial}{\partial \theta} \left(\sin(\theta) \frac{\partial f}{\partial \theta} \right) + \frac{1}{r^2 \sin^2(\theta)} \frac{\partial^2 f}{\partial \phi^2}$$

$$\hat{Z}_i(z) = \hat{\eta}_i \frac{1 + \hat{\Gamma}_i(z)}{1 - \hat{\Gamma}_i(z)} \quad , \quad \hat{\Gamma}_i(z) = \frac{\hat{Z}_i(z) - \hat{\eta}_i}{\hat{Z}_i(z) + \hat{\eta}_i} \quad \&$$

$$\hat{\Gamma}_i(z') = \hat{\Gamma}_i(z) e^{2\hat{\gamma}_i(z'-z)} \quad \text{where } z' \& z \text{ are two positions in } i^{\text{th}} \text{ region}$$